SANTA ANA RIVER WATERMASTER

FOR

ORANGE COUNTY WATER DISTRICT Vs. CITY OF CHINO, et al

CASE No. 117628 - COUNTY OF ORANGE

FOURTH

ANNUAL REPORT

OF THE

SANTA ANA RIVER WATERMASTER

1973-74

FEBRUARY 18, 1975

SANTA ANA RIVER WATERMASTER

FOR ORANGE COUNTY WATER DISTRICT VS. CITY OF CHINO, ET AL CASE NO. 117628 – COUNTY OF ORANGE

WATERMASTER
MAX BOOKMAN
WILLIAM J. CARROLL
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ALBERT A. WEBB

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February 18, 1975

To:

Clerk of Superior Court of Orange County

and all Parties

Re:

Watermaster Report for 1973-74

Gentlemen:

We have the honor of submitting the fourth annual report of the Santa Ana River Watermaster.

The principal findings of the Watermaster for the water year 1973-74 are as follows:

At Prado

(2)	Base Flow at Prado Annual Weighted TDS of Total Flow Annual Adjusted Base Flow	43,769 acre-feet 704 ppm 43,769 acre-feet
(4)	Cumulative Adjusted Base Flow	174,118 acre-feet 168,000 acre-feet
(5) (6)	Cumulative Entitlement of OCWD at Prado Cumulative Credit (4)-(5)	6,118 acre-feet
(7)	One-third of Cumulative Debit Minimum Required Base Flow in 1974-75	0 acre-feet 37,000 acre-feet
(8)	Minimum Required Dase 110w m 17/12	•

At Riverside Narrows

(1)	Base Flow at Riverside Narrows	16,203 acre-feet
(2)	Annual Weighted TDS of Base Flow at	700 ppm
	Riverside Narrows	16,203 acre-feet
(3)	Annual Adjusted Base Flow	•
(4)	Cumulative Adjusted Base Flow	66,337 acre-feet
(5)	Cumulative Entitlement of CBMWD and	
. (-/	WMWD at Riverside Narrows	61,000 acre-feet
163	Cumulative Credit	5,337 acre-feet
(6)		0 acre-feet
(7)	One-third of Cumulative Debit	13,420 acre-feet
(8)	Minimum Required Base Flow in 1974-75	15,420 acre-rect

The above findings show that at the end of the water year 1973-74 there existed a credit of 6,118 acre-feet in the obligations of Chino Basin Municipal Water District and Western Municipal Water District in the discharge of Base Flow downstream from Prado Dam. During the following water year, 1974-75, the minimum required Base Flow is 37,000 acre-feet. At Riverside Narrows, there existed a credit of 5,337 acrefeet. The obligation of San Bernardino Valley Municipal Water District during the water year 1974-75 is a minimum Base Flow of 13,420 acre-

-2-

During the water year 1973-74 Nontributary water was released from the California Aqueduct at Devil Canyon Powerplant to the Rialto Feeder of The Metropolitan Water District. These releases were made at the request of the Orange County Water District. The Nontributary water purchase was for ground water replenishment in Orange County. An appropriate adjustment was made to exclude this Nontributary water in the determination of Base Flow and Adjusted Base Flow at Prado Dam. Similarly an appropriate adjustment was made for that portion of Nontributary water released above Riverside Narrows during water year 1972-73 which reached Prado during the water year 1973-74.

Sincerely yours,

Santa Ana River Watermaster

By: Max Bookman

James C. Hanson

Albert A. Webb

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SANTA ANA RIVER WATERMASTER



Max Bookman Chairman



Albert A. Webb Secretary



James C. Hanson



William J. Carroll



John M. Toups

CHAPTER I INTRODUCTION

On October 1, 1970 as the result of the stipulated Judgment in Case No. 117628, Orange County Water District vs City of Chino, et al, entered on April 17, 1967, a regional allocation of the water supply of the Santa Ana River became effective which established entitlements to the river supply as between the Upper Area in San Bernardino and Riverside Counties, and the Lower Area in Orange County. In addition to a declaration of rights the Judgment also contains provisions for a physical solution to implement the agreement reached. The obligations to maintain the flow of the river at specified annual amounts at Riverside Narrows and Prado are placed on certain parties to the Judgment. The parties named in the Judgment are the four major public water districts within the Santa Ana River Watershed; namely, the San Bernardino Valley Municipal Water District, Western Municipal Water District of Riverside County, Chino Basin Municipal Water District and Orange County Water District.

In order to administer the provisions of the Judgment the Court appointed a Watermaster composed of five persons and required that the Watermaster report annually to the Court and the Parties. During the 1973-74 water year the Santa Ana River Watermaster Committee consisted of Max Bookman, William J. Carroll, James C. Hanson, John M. Toups and Albert A. Webb. Mr. Bookman served as Chairman and Mr. Webb performed the functions of Secretary. This report for the water year 1973-74 is the fourth annual report to be issued since the Judgment became effective.

Scope of Report

Section 7(c) of the Judgment requires the Watermaster to report to the Court and to each party not more than five months after the end of each water year starting with 1970-71. The items to be reported upon are as follows:

- (a) Prado Accounting
 - (1) Base Flow at Prado
 - (2) Annual Weighted TDS of Total Flow at Prado
 - (3) Annual Adjusted Base Flow
 - (4) Cumulative Adjusted Base Flow

- (5) Cumulative Entitlement of OCWD at Prado
- (6) Cumulative Credit or Debit
- (7) One-third of Cumulative Debit
- (8) Minimum Required Base Flow in Following Year
- (b) Riverside Narrows Accounting
 - (1) Base Flow at Riverside Narrows
 - (2) Annual Weighted TDS of Base Flow at Riverside Narrows
 - (3) Annual Adjusted Base Flow
 - (4) Cumulative Adjusted Base Flow
 - (5) Cumulative Entitlement of CBMWD and WMWD at Riverside Narrows
 - (6) Cumulative Credit or Debit
 - (7) One-third of Cumulative Debit
 - (8) Minimum Required Base Flow in Following Year

The above listed items as determined by the Watermaster for the water year 1973-74, in addition to other data compiled by the Watermaster, are hereinafter set forth. This first chapter is followed by Chapter II, "Prior Year Activities", Chapter III, "Water Supply Conditions", Chapter IV, "Base Flow at Prado", and Chapter V, "Base Flow at Riverside Narrows". As a matter of information, the Appendices of this report contain a brief history of the litigation, a summary of the Judgment, a summary of Nontributary flow and records of water quality below Prado Dam and at Riverside Narrows.

CHAPTER II

PRIOR YEAR ACTIVITIES

While the water supply in the Santa Ana River during the 1973-74 water year decreased as a result of below normal precipitation in the watershed, there was a major increase in the Nontributary water purchased by the Orange County Water District but delivered in the Upper Area and transported through pipelines and natural channels downstream through Prado Dam to the Lower Area.

Four Watermaster meetings were held during 1974. All meetings were held in the offices of the Watermaster in Riverside. Copies of the minutes of the meetings held are available for public inspection in the Watermaster office.

As required by the Judgment the Watermaster prepared the "Third Annual Report of the Santa Ana River Watermaster, 1972-73" which was published under date of February 15, 1974 and copies were submitted to the Court and the Parties. The Watermaster continued the work of collection and analyses of data, maintenance of records and preparation of the 1973-74 annual report. The Watermaster also compiled records and accounts for the Nontributary water from the State Water Project released in the Upper Area at the request of the Orange County Water District. This chapter will describe the Watermaster activities and briefly summarize important related activities of the four major public water districts in the watershed.

Watermaster Service

Stream Flow and Water Quality Measurements

Services to provide the stream flow measurements and water quality data required by the Watermaster were for the most part furnished by the U.S. Geological Survey (USGS). Additional data related to the operation of Prado Reservoir were obtained from the Corps of Engineers and water quality data were supplied to the Watermaster by the State Department of Water Resources, the Riverside and Corona City Sanitation Departments and the Chino Basin Municipal Water District. Data regarding the discharge of Nontributary water into the Santa Ana River were provided by the Metropolitan Water District and the State Department of Water Resources. The financing of the cooperative monitoring program with the USGS was shared by the parties to the Judgment. Such costs are set forth in Table 1.

TABLE 1

COSTS TO THE PARTIES AND USGS FOR MEASUREMENTS WHICH PROVIDE DATA USED BY THE SANTA ANA RIVER WATERMASTER July 1, 1973 to June 30, 1974

SAN BERNARDINO VALLEY MUNICIPAL WATER DISTRICT

At Riverside Water Quality Control Plant Surface Water Gage Water Quality Monitor TDS Samples	\$ 290.00 500.00 90.00	
At MWD Crossing Water Quality Monitor TDS Samples Dozer	520.00 90.00 83.00	
At Prado Park	312.00	
At Mission Boulevard	240.00	
Analysis, Data Preparation, and Counsel to Santa Ana River Watermaster	 600.00	\$ 2,725.00
WESTERN MUNICIPAL WATER DISTRICT		
Same as SBVMWD (\$1.00 difference due to rounding) Temescal Creek Discharge Cucamonga Creek Discharge Chino Creek Discharge	\$ 2,726.00 513.00 513.00 512.00	4,264.00
CHINO BASIN MUNICIPAL WATER DISTRICT		
Same As WMWD (\$2.00 difference due to rounding)		4,262.00
ORANGE COUNTY WATER DISTRICT		
At Prado Dam Water Quality Monitor, Conductivity Program, and Counsel to Santa Ana River Watermaster TDS Determination At Prado Park At Mission Boulevard	\$ 8,080.00 800.00 624.00 480.00	9,984.00
TOTAL FOR PARTIES		\$21,325.00
UNITED STATES GEOLOGICAL SURVEY	•	21,235.00
GRAND TOTAL		\$42,470.00

The USGS measured and computed the mean daily discharge of the Santa Ana River at Mission Boulevard, MWD Crossing, Prado Park, and Below Prado Dam as well as the daily discharge of the Riverside Water Quality Control Plant into the Santa Ana River. Discharge measurements were also provided for three smaller streams tributary to Prado Reservoir; Temescal Creek at Corona, Chino Creek at Schaefer Avenue and Cucamonga Creek near Mira Loma.

The U.S. Geological Survey reported that during 1974 the newly constructed low-water control at the gaging station Santa Ana River at MWD Crossing worked well, and provided the data which resulted in an improved record of the discharge. This control has permitted the collection of good data at a normally poor site. The gaging station Temescal Creek at Corona was discontinued on September 30, 1974. This station will have to be relocated if the collection of discharge data is to be continued at this site. Sampling of the Nontributary water in San Antonio Creek commenced on March 28, 1974 for standard cations and anions. As part of this program samples of the water at the Chino Creek gaging station were also taken.

Water quality data are also collected at monitoring stations located at MWD Crossing, Riverside Water Quality Control Plant, and Below Prado Dam.

Compilation and Analysis of Basic Data

The watermaster has established records and procedures for compiling and analyzing the basic data necessary in order to carry out the provisions of the Judgment. These records include the following:

- (1) Daily precipitation at San Bernardino County Hospital.
- (2) Flow of Santa Ana River at USGS gaging station Below Prado Dam.
- (3) Flow of Santa Ana River at USGS gaging station at Prado Park.
- (4) Flow of the Santa Ana River at MWD Crossing.
- (5) Discharge of Riverside Water Quality Control Plant into the Santa Ana River.
- (6) Flow of the Santa Ana River at Mission Boulevard Bridge.
- (7) Specific conductance and TDS of the waters of the Santa Ana River Below Prado Dam.
- (8) Specific conductance and TDS of the waters of the Santa Ana River at MWD Crossing.
- (9) Specific conductance and TDS of the discharge of the Riverside Water Quality Control
- (10) U.S. Army Corps of Engineers Records of Water Storage at Prado Dam.
- (11) Flow of Chino Creek at Schaefer Avenue.

- (12) Discharge of San Bernardino Water Quality Control Plant into the Santa Ana River.
- (13) Flow of Temescal Creek at Corona.
- (14) Water Quality Analysis of samples taken at San Antonio Creek and Chino Creek.
- (15) Daily evaporation at Riverside Citrus Experimental Station.
- (16) Discharge of Nontributary water released at Devil Canyon.
- (17) Discharge of Chino Basin MWD Water Quality Control Plant at Chino Creek.
- (18) Discharge of Chino Basin MWD Water Quality Control Plant to 30-inch outfall line to Prado Flood Basin.
- (19) Discharge of City of Corona Water Quality Control Plant to Temescal Creek,
- (20) Daily precipitation at several recording Stations above Prado Dam.

Based on these compiled data, determinations were made of Base Flow, Storm Flow, Nontributary water and relationships between specific conductance and TDS. These determinations are explained in detail in Chapters IV and V.

Administration Costs

In accordance with Paragraph 7(d) of the Judgment, the fees and expenses of each of the members of the Watermaster are to be borne by the district which nominated such member. All other Watermaster administrative costs and expenses are borne by the parties, with OCWD assuming 40 percent of the cost and CBMWD, SBVMWD and WMWD each bearing 20 percent of the cost. The Judgment further provides that the Watermaster may from time to time, in its discretion, require advances of operating capital from the parties.

At its meeting on June 5, 1973 the Watermaster adopted a budget for the fiscal year 1973-74 in the amount of \$30,000, of which \$17,000 was estimated to be required for additional gaging and monitoring expenses. A special item of \$10,000 was added to the budget for the extra engineering and monitoring related to the release of Nontributary water, the cost of which was to be borne by Orange County Water District. Table 2 shows the items and amounts included in said budget.

TABLE 2
SANTA ANA RIVER WATERMASTER BUDGET

	July 1, 1973 to June 30, 1974	July 1, 1974 to June 30, 1975
Administration	\$ 3,000.00	\$ 2,000.00
Supporting Engineering Services	10,000.00	5,000.00
Reproduction of Annual Report		1,500.00
Additional gaging and monitoring stations, including construction, operation and maintenance	17,000.00 \$ 30,000.00	\$ 8,500.00
ORANGE COUNTY WATER DISTRICT - Extra engineering relative to release of State water	10,000.00	
Total	\$ 40,000.00	\$ 8,500.00

Table 3 is a statement showing the income and expenses of the Santa Ana River Watermaster for the fiscal year 1973-74. The expenses as shown total \$31,836.87, comprised of \$7,918.42 of normal operating costs, \$12,000 for construction of a weir at the Riverside Narrows gage and \$11,918.45 for a special investigation of Nontributary water.

Related Activities of Other Agencies

San Bernardino Valley Municipal Water District

State Project water has continued to flow into the spreading basins in the Upper Santa Ana River from the San Bernardino Valley Municipal Water District's Master Distribution System. Three turnouts in Phase I, Devil Canyon to Waterman Canyon, have been used in this initial delivery; Phase II, Waterman Canyon to Santa Ana River, is now under construction.

Phase II will add an additional 60,000 feet of 78-inch diameter pipeline with turnouts at strategic locations for spreading into existing stream beds and spreading grounds as well as delivery capability to customers who wish to take raw water directly from the pipeline. Additional facilities for future connections are part of Phase II and located in cooperation with other agencies in the San Bernardino Valley.

TABLE 3

INCOME AND EXPENSES July 1, 1973 - June 30, 1974

INCOME

Balance June 30, 1973 Payments by Parties for Fiscal 1973-74 Chino Basin Municipal Water District Orange County Water District San Bernardino Valley Municipal Water District Western Municipal Water District Orange County Water District (Special Assessment - Nontributary Water Investigation and Report)	\$ 4,000.00 8,000.00 4,000.00 4,000.00	\$14,651.31
Total Balance June 30, 1973 plus Income Fiscal 1973-74		\$46,569.76
EXPENSE		
Secretary - Office Expense	\$ 1,385.48	
Bookman-Edmonston Engineering, Inc. Preparation of 1972-73 Annual Report, including graphs and diagrams	1,038.05	
James C. Hanson Preparation of Prado hydrograph; work on Annual Report; work on MWD Crossing control plans, including meetings with contractor, inspection of construction, and meetings with USGS	953.15	
Albert A. Webb Associates Preparation of data from U.S. Corps of Engineers for Prado Reservoir surface charts; work on Annual Report; preparation of Riverside Narrows hydrograph	3,426.27	
Albert A. Webb Associates Nontributary Water Investigation and Report	11,918.45	
James M. Montgomery, Consulting Engineers, Inc. Printing of 1972-73 Annual Report	1,115.47	
E. L. Yeager Construction Company, Inc. Weir construction at MWD Crossing	12,000.00	31,836.87
Balance June 30, 1974		\$14,732.89



Part of San Bernardino Valley Municipal Water District's distribution system for State Project water showing spreading basins and the proximity of the new pipeline. (SBVMWD Photo 4134)

Construction of Phase II is approximately 35% complete. Major flood channel crossings were completed prior to the winter season. Spreading grounds and areas affected by construction have been restored so runoff can be controlled with minimum interference and erosion.

To aid in basin management, the District has begun to assemble a hydrologic computer data base. This data base contains current and historic well measurements, water quality data, amounts of precipitation, production, stream flows, amounts of import and export. Input to the data base is basically from two sources: (1) local agencies who voluntarily contribute data and (2) District operated monitoring programs. At present, the District monitors surface and ground water for changes in water quality at 45 locations. In addition, District personnel measure 80 wells on a monthly basis. In 1974 the Western and San Bernardino Valley Municipal Water Districts through the Western-San Bernardino Watermaster established a rain gage network to monitor the precipitation in the Bunker Hill-San Timoteo Basins. Hydrologic data input to the data base is retrieved for utilization in the various District reports published throughout the year.

Western Municipal Water District of Riverside County

During 1974, the Western Municipal Water District of Riverside County, acting as the regional agency for Jurupa Community Services District, Rubidoux Community Services District, and the City of Riverside, in order to comply with the California Regional Water Quality Control Board's orders for additional treatment of wastes (tertiary treatment) for the area, held a General Obligation bond election in November, receiving 53.9 percent of the vote. This was short of the necessary two-thirds vote. Meetings were held following the election, and new proposals by the three agencies were submitted to the California Regional Water Quality Control Board.

Western Municipal Water District of Riverside County became a full member of the Santa Ana Watershed Project Authority the latter part of the year.

The Metropolitan Water District of Southern California completed, during the year, its Environmental Impact Reports and public hearing on the Riverside Filtration Plant and the Box Springs Feeder. This latter project will provide the capability of blending State Project Water and Colorado River Water in the Lower Feeder. The MWD Board authorized the construction of these facilities, with the Box Springs Feeder to be operational in the early part of 1977.

Chino Basin Municipal Water District

The activities of CBMWD have been quite varied this year, with most of the attention being directed toward the solution of the wastewater problems prevalent in the District.

In the middle of July of 1974 the Cucamonga Interceptor was completed and connected to the CBMWD Regional Plant No. 1, with the result that an additional one to two million gallons per day of treated effluent is now being discharged to the Santa Ana River. Also grant funding was secured for the Montclair Interceptor, which when completed will deliver approximately 1.5 mgd of wastewater, now going to Los Angeles County, to Plant No. 1 and, hence, to the Santa Ana River.

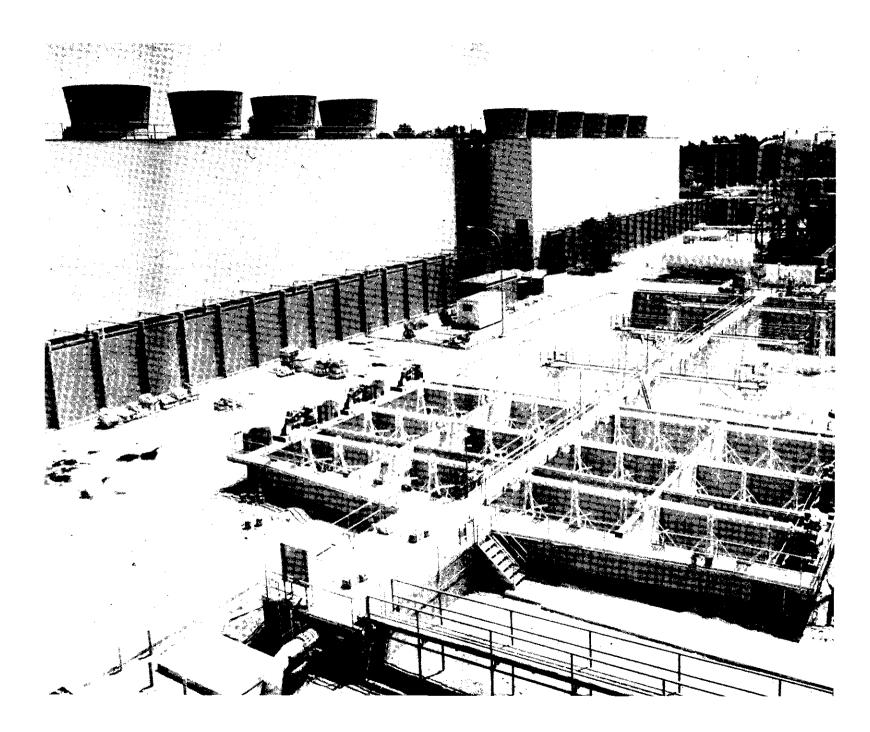
Regional Plant No. 2 (previously City of Chino plant) also is being studied and the design of additions and improvements has been authorized. The improvement will consist of enlarging the plant to an average capacity of 5 mgd and modifying the process to accomplish complete nitrification and partial denitrification. A tertiary plant will also be designed and constructed at this site. A pilot plant study for the use of ozone as a disinfectant and a substitute for chemical coagulation and sedimentation prior to filtration is now being conducted at this site.

Two items involving water management were worked on during the year but were not completed. One is an amendment to CBMWD's authorization act to permit a pump tax on ground water. It is expected that this will be considered by the State Legislature early in 1975. The second is a ground water adjudication of the Chino Basin. A complaint was filed in the Superior Court of the State of California, County of San Bernardino, on January 2, 1975. This complaint asked for adjudication of water rights, for injunctive relief and for physical solution. The plaintiff is CBMWD, with the defendants being six cities, nine public districts, the State of California, 44 water companies, 169 business entities, 1,624 individuals and 2,000 John Does. It is expected that the adjudication procedure will be essentially a friendly one, with the end result serving as a basis for more complete management of the water resource system of the Chino Basin area.

Orange County Water District

The Orange County Water District continued their efforts to supplement the natural replenishment and to protect the groundwater supplies of Orange County.

Water Factory 21, the District wastewater reclamation-sea water desalting plant was under construction. At the end of the water year, the desalter was approximately 97% complete and the wastewater reclamation plant was approximately 98% complete. The well injection system was



Water Factory 21

completed in the prior water year. The water from the two processes will be blended and supplied to the coastal barrier project in the Huntington Beach-Fountain Valley area to prevent further sea water intrusion and provide a supplemental water supply.

The District has initiated the design of two projects which will become components of Water Factory 21 and will provide an interim, additional freshwater supply. The projects consist of the design of three deep wells, with a total design capacity of 6 mgd, and the design of a membrane demineralizer, which will demineralize a portion of the product water from the reclamation plant.

The District continued its water conservation operations at Anaheim Lake and the spreading areas within and adjacent to the Santa Ana River. During the past year, 49,478 acre-feet of imported Colorado River water were released for spreading at Anaheim Lake and adjacent spreading facilities. During the same period, 65,078 acre-feet of imported State Water Project water were released above Prado Dam for conveyance to spreading facilities in Orange County.

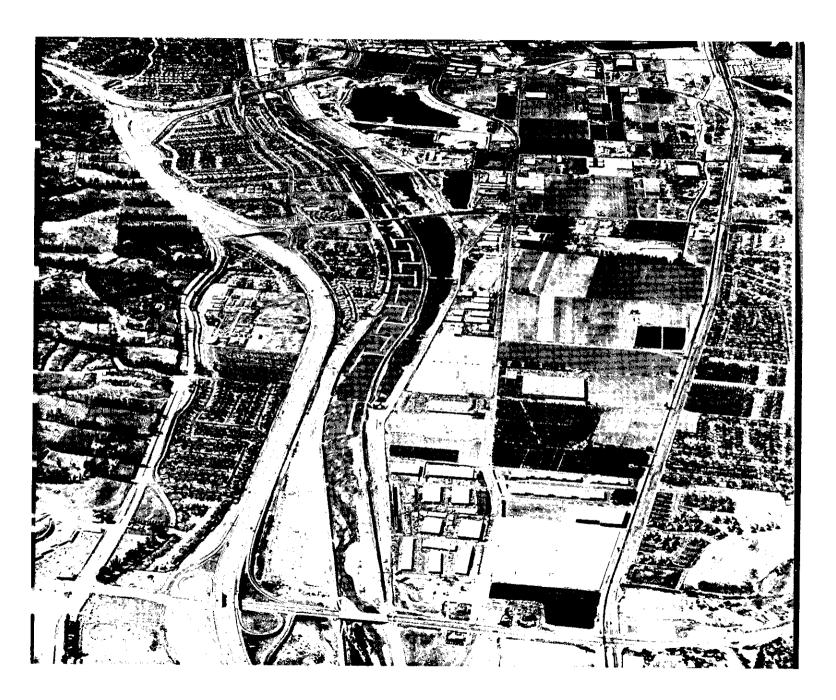
Water conservation facilities adjacent to the Santa Ana River between Imperial Highway and Lakeview Avenue were improved during the water year. Three concrete overflow weirs, a Parshall Flume, protective housing, and other miscellaneous improvements were constructed. This area will be utilized for desilting and spreading flows diverted from the Santa Ana River.

In cooperation with USGS, flow measurement stations have been established at the Parshall Flume and at a location within the Santa Ana River downstream of the structure which diverts flows to the Parshall Flume.

Subsequent to the water quality management study by the Santa Ana Watershed Planning Agency, the District initiated a study to update its master plan for spreading grounds. The objective of the master plan is to conserve the optimum amounts of the large quantities of water which will be available in the future for groundwater replenishment.

To gain greater flexibilities in the operations of the spreading grounds, the District began construction of a 66-inch pipeline between the Santa Ana River and Anaheim Lake. The design of an outlet structure at Anaheim Lake was also initiated in order to spread State water at Orange County Flood Control District facilities downstream of Anaheim Lake.

The District continued studies of pilot desalting facilities to demineralize the effluent from the proposed Anaheim Watewater Reclamation Plant to be built by the District and County Sanitation Districts of Orange County. The potential project will develop greater utilization of present supplies and improve groundwater quality.



Spreading basins in Santa Ana River in Orange County

Santa Ana Watershed Planning Agency and Santa Ana Watershed Project Authority

Previous annual reports of the Watermaster have described the establishment and progress of the Santa Ana Watershed Planning Agency (SAWPA), a joint powers entity, formed by the Chino Basin Municipal Water District, Orange County Water District, San Bernardino Valley Municipal Water District and Western Municipal Water District. The purpose for the Planning Agency, stated in 1967, was the development of a comprehensive water quality management plan for the Santa Ana River Watershed. Plan development encompassed all known planning by local entities, cognizance of the Stipulated Judgment and the Watermaster role in the Watershed, and anticipation of both Regional and State activities with respect to local and imported waters, from both the State Project and the Colorado River systems. A key element in the plan is to increase the use of high quality State Project water and to decrease the use of Colorado River water.

In April, 1974, SAWPA delivered to the Environmental Protection Agency, Region IX, the 3-C report which represented completion of a federal clean water planning grant. These funds were matched by local funds from the four member agencies. The 3-C report was followed in late September of 1974 by delivery of a Water Quality Control Plan to the State and Regional Water Quality Control Boards. When finalized and adopted, this latter plan will take the place of the Interim Plan administered by the Regional Board and will set new water quality objectives on many waters within the Santa Ana Basin. Changes in the Santa Ana Watershed include mineral quality objectives for surface flow near Prado Dam and for groundwater subbasins in the Upper and Lower Watersheds. The San Jacinto Watershed will have beneficial use definition and water quality objectives for specific surface and underground waters for the first time as a result of the Water Quality Control Plan.

To date, the cost of development of these plans has been approximately \$1,250,000. Of this, about \$610,000 has been provided by federal and state clean water agencies, with the remaining \$640,000 being provided by the local participating districts.

The Planning Agency has been succeeded in interest by the Santa Ana Watershed Project Authority, with the four major water districts as members. These four districts are continuing their efforts for comprehensive and coordinated management of water quantity and quality within the Santa Ana River Watershed.

As evidence of this coordinated effort, the parties have under construction, in cooperation with the County Sanitation Districts of Orange County, the Santa Ana Regional Interceptor. This \$25 million salinity control pipeline represents the key salt removal element envisioned by the planning efforts.

CHAPTER III

WATER SUPPLY CONDITIONS

The 1973-74 precipitation in the watershed was below normal which adds to the large deficiency in water supply experienced during the last five years since the unusually high precipitation experienced in 1968-69. Accordingly, the total flow in the Santa Ana River during the water year 1973-74 decreased. In addition to the decrease in Storm Flow at Prado, the Base Flow also decreased. This decrease in Base Flow was partly offset by the increased discharge of treated wastewater into Prado Reservoir from the Ontario-Upland Treatment Plant in the Chino Basin.

Precipitation During 1973-74

During the 1973-74 water year the precipitation at the San Bernardino County Hospital amounted to 12.72 inches, which is 71 percent of the Base Period average. Most of the precipitation occurred during the months of January and March with monthly amounts of 6.88 inches and 3.00 inches respectively.

Figure 1 shows the seasonal precipitation from 1931-32 through 1973-74 and the accumulated departure from the 1934-35 through 1959-60 Base Period average.

Runoff During 1973-74

Below Prado Dam

The total flow of the Santa Ana River at Prado Dam, less Nontributary water, during 1973-74 was 63,312 acre-feet, which is below the 26-year Base Period (1934-35 through 1959-60) average of 78,780 acre-feet per year. This compares to the flow during the prior year of 77,484 acre-feet when a greater amount of precipitation occurred.

The Base Flow at Prado Dam decreased progressively during the extended drought period and reached a low in 1960-61 of 26,190 acre-feet. Since that year, the Base Flow has generally increased. During 1969-70 the Base Flow amounted to 39,075 acre-feet. The below normal rainfall of the 1970-71 water year was evidenced by a decline in the Base Flow to 38,402 acre-feet; however, during 1971-72 it had again risen to 40,416 acre-feet. During 1972-73 the Base Flow increased to 48,999 acre-feet as compared to the 26-year Base Period average of 47,470 acre-feet. However, during the current year 1973-74 the Base Flow dropped to 43,769 acre-feet.

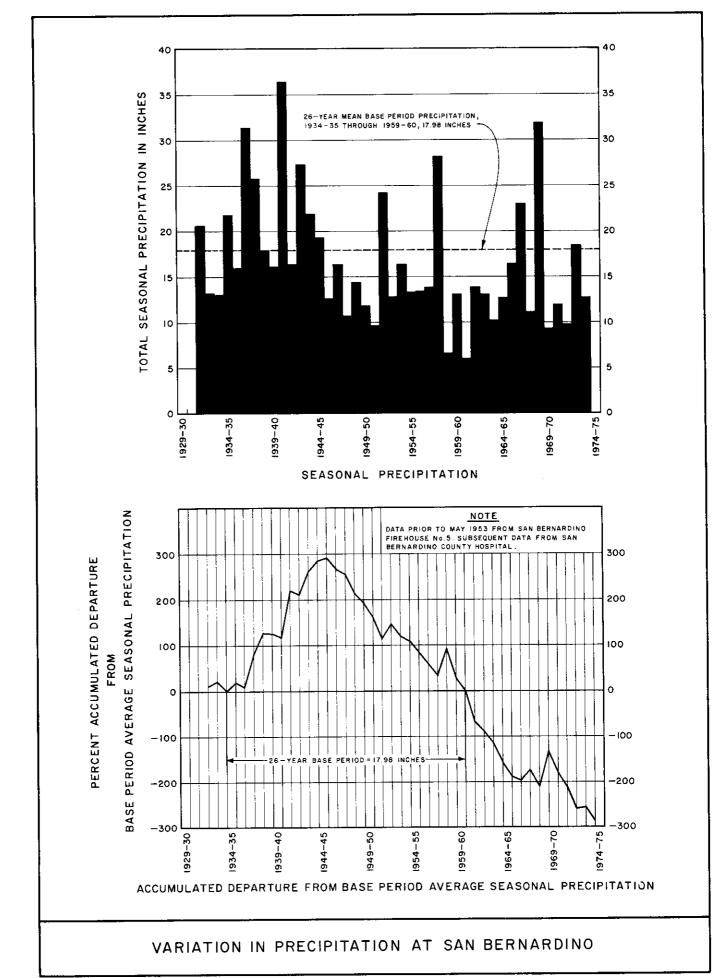


Figure 2 shows the Storm and Base Flow components of the Total Flow in the Santa Ana River below Prado Dam.

At Riverside Narrows

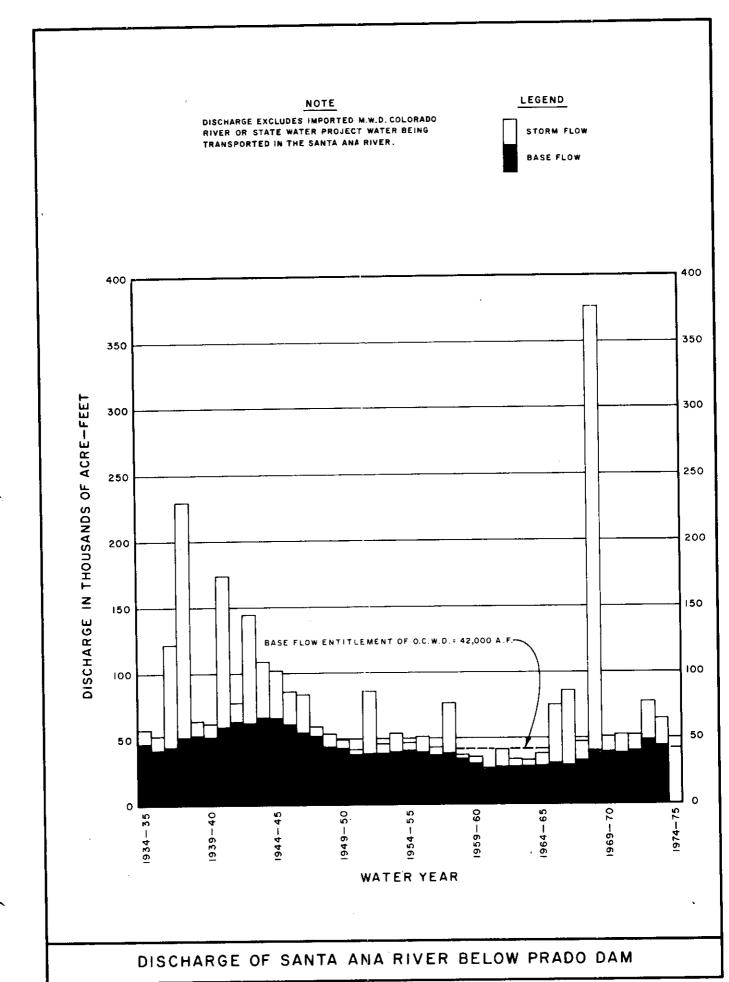
The total natural flow (excluding City of Riverside's sewage effluent and State Project water) at Riverside Narrows for the 1973-74 water year was again below the 26-year Base Period average, amounting to 24,494 acre-feet as compared to the Base Period annual average of 44,650 acre-feet.

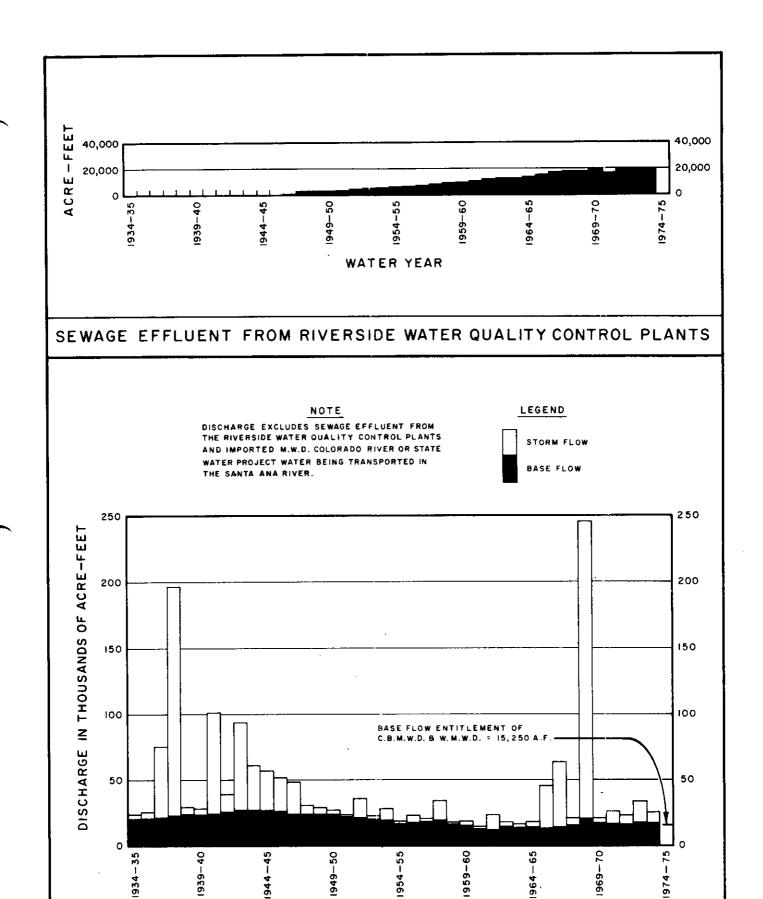
The Base Flow at Riverside Narrows decreased from 27,120 acre-feet in 1943-44 to 16,410 acre-feet in 1954-55, increased to 19,470 acre-feet in 1957-58, then decreased to an all-time low of 13,450 acre-feet in 1965-66. Since that time the Base Flow at Riverside Narrows gradually increased to 17,223 acre-feet in 1969-70. The Base Flow at Riverside Narrows decreased to 17,061 acre-feet in 1970-71, to 16,157 acre-feet in 1971-72, increased to 17,105 acre-feet in 1972-73 and decreased to 16,203 acre-feet in 1973-74. This amount compares to the 26-year Base Period annual average of 22,190 acre-feet.

Figure 3 shows the components of natural flow in the Santa Ana River at Riverside Narrows and the sewage effluent from the Riverside Water Quality Control Plant for the period from 1934-35 through 1973-74.

Sewage Effluent from Riverside Water Quality Control Plants

Since the late 1940's the sewage effluent from the Riverside Water Quality Control Plants, which is discharged at the Riverside Narrows between Pedley Bridge and the MWD Crossing, has been increasing in amount. In 1949-50, the amount of treated effluent from Riverside No. 1 and No. 2 plants was 3,960 acre-feet. By 1959-60, the discharge from these plants had increased to 9,900 acre-feet. By 1969-70, the discharge of sewage effluent from the combined treatment plants was 18,657 acre-feet. Thus the contribution of wastwater flow effluent by the City of Riverside has been increasing at a rate of about 800 acre-feet per year. This trend is illustrated on Figure 3. The wastewater flow discharge of the Riverside Water Quality Control Plants during 1973-74 was 19,561 acre-feet. The total for the wastewater flow and the total natural flow of 24,494 acre-feet amounts to 44,055 acre-feet.





WATER YEAR

Effluent from Ontario-Upland Wastewaster Treatment Plant

In late December 1971 and continuing to date, wastewater effluent from the recently constructed tertiary plant serving Ontario and Upland has been discharged through a 30-inch pipeline and ditch to Prado Reservoir. The quantity of effluent during the water year 1973-74 amounted to about 11,435 acre-feet.

Source of Water Supply at Prado Dam

Prior to the regional allocation of water accomplished under the Judgment, the flow in the Santa Ana River reaching Prado Dam originated as a result of storm runoff and rising water. Using the Base Period 1934-35 through 1959-60 for negotiating purposes, agreement between the parties to the Judgment determined that the Base Flow entitlement of Orange County Water District, in the future, should average 42,000 acre-feet. As stated, historically the Base Flow was comprised of rising water; however, under the Judgment, Base Flow is defined as that portion of the total surface flow passing a point of measurement which remains after deduction of storm flow. As discussed herein, in more recent years treated wastewater has been discharged to the River from a number of wastewater treatment plants. It is interesting to note that during the water year 1973-74 the discharge to the River from the Riverside Quality Control Plants, the Ontario-Upland Sewage Plant, and the Corona Sewage Treatment Plant total 34,503 acre-feet. The total amount of Base Flow at Prado Dam during this year amounted to 43,769 acre-feet.

CHAPTER IV BASE FLOW AT PRADO

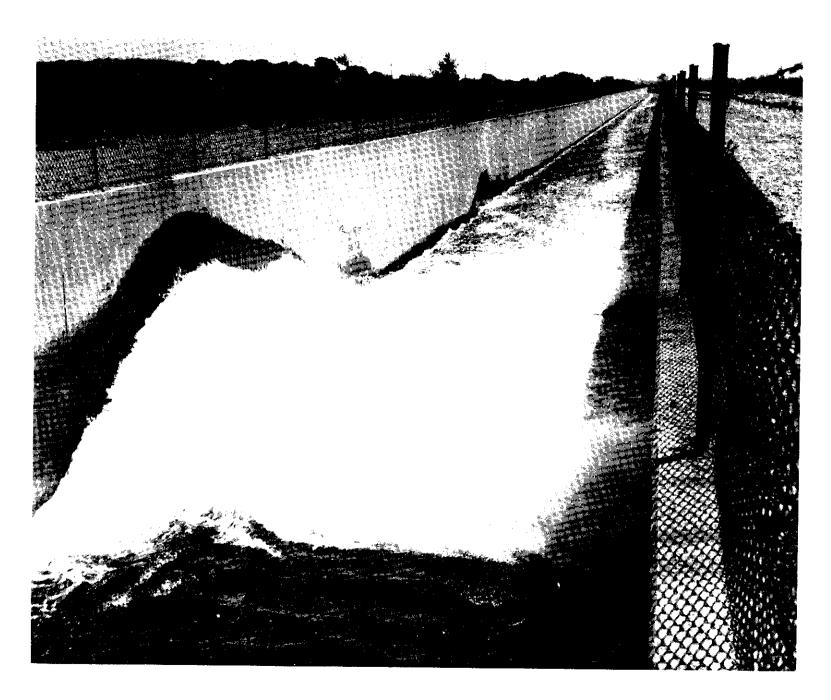
This chapter deals with the analysis of the flow at Prado Dam, the calculation of the amount of Base Flow at Prado credited to CBMWD and WMWD, and the calculation of the Adjusted Base Flow. The adjustment of Base Flow is made on the basis of the weighted average annual TDS of the total flow at Prado less any Nontributary water.

Total Discharge at Prado

The total discharge of the Santa Ana River at Prado during 1973-74 water year amounted to 128,436 acre-feet, as measured at the USGS gaging station below Prado Dam. This amount includes the State water released into San Antonio Creek during 1973-74 and additional rising water from the Riverside groundwater basin due to the release of State water into Santa Ana River during 1972-73. The members of the Watermaster agreed to adjust this amount to 127,327 acre-feet in order to subtract the 1,109 acre-feet of water which were in storage on September 30, 1973, but credited as Base Flow in 1972-73. Because of the large quantities of State water, the total discharge at Prado cannot be compared to the 26-year average annual flow of 78,780 acre-feet during the Base Period of 1934-35 through 1959-60 as in previous years. During the water year 1973-74, a minimum monthly discharge of 4,548 acre-feet occurred in October and a maximum monthly discharge of 22,082 acre-feet occurred in January.

Components of Flow

Of the total discharge at Prado during the 1973-74 water year, 43,769 acre-feet were Base Flow, 19,543 acre-feet were Storm Flow, 980 acre-feet were Nontributary flow due to the release of State Water Project water into the Santa Ana River in 1972-73, and 63,035 acre-feet were Nontributary flow due to State water released into San Antonio Creek. The components of flow were independently determined by each of the five members of the Watermaster using the general procedure set forth in the Work Papers of the engineers for the parties in reaching the physical solution provided for in the Judgment. The Base Flow of 43,769 acre-feet represents an average value of the computations submitted by the five members of the Watermaster. Details of the scalping procedure are described in the following section and the results are graphically shown on



Delivery of State Project Water into San Antonio Wash in Montclair (Connection OC 59-T)

Plate 2. The components of flow of the Santa Ana River at Prado Dam for each month in the 1973-74 water year are listed in Table 4.

TABLE 4

COMPONENTS OF FLOW AT PRADO DAM

FOR WATER YEAR 1973-74

(Acre-Feet)

	USGS	Change	200			Nontributary Water	
Month	Measured Outflow	in Storage	Computed Inflow	Storm Flow	Base Flow	San Antonio Creek*	Riverside Narrows**
	4.540	1 100	2 420	0	3,358	0	81
Oct 73	4,548	-1,109	3,439	1,196	3,793	ŏ	81
Nov	5,070		5,070		•	6,812	81
Dec	11,530	+ 1	11,531	87	4,551	0,012	01
	21.004	+ 208	22,092	13,892	5,427	2,692	81
Jan 74	21,884		,	97	4,923	7,166	82
Feb	12,468	- 200	12,268		,	1,645	82
Mar	11,088	- 9	11,079	3,543	5,809	1,043	02
	7.071	1	7,860	393	4,306	3,079	82
Apr	7,861	+ 3	9,294	335	3,820	5,057	82
May	9,291	+ 3	•	0	2,755	7,535	82
June	10,372		10,372	U	2,733	1,555	02
T .1	12 577	+ 6	12,583	0	1,446	11,055	82
July	12,577		,	ŏ	1,677	11,776	82
Aug	13,539	- 4	13,535		1,904	6,218	82
Sep	8,208	<u> </u>	8,204	0	1,904	0,210	<u></u>
Totals	128,436	-1,109	127,327	19,543	43,769	63,035	980

^{*}State water released into San Antonio Creek through Devil Canyon during 1973-74, including adjustments for conveyance losses.

Operation of Prado Dam and Reservoir

During the 1973-74 water year, water was stored behind Prado Dam during the periods October 1 to October 6; November 18 to November 28; December 5 to December 14; January 4 to January 19; January 28 to January 31; February 5 to February 7; March 2 to March 30; and April 1 to April 3. During these periods, the water stored in Prado Reservoir varied up to a maximum of 4,875 acre-feet and the maximum mean daily flow released to the Santa Ana River was 1,420 cfs.

Generally during storms, the Corps of Engineers operated the Prado gates so that some of the storm runoff was temporarily held in storage behind the dam. As the storm ended, Prado Reservoir

^{**}That portion of State water released during water year 1972-73 upstream of Riverside Narrows, assumed to have reached Prado Dam in 1973-74.

storage was gradually reduced by the controlled releases to the downstream water conservation facilities operated by Orange County Water District. The Prado gates were closed on September 17, 1973 and remained closed until October 1, 1973 in order to make repairs downstream of the dam. The 1,109 acre-feet in storage on September 30, 1973 was considered to be Base Flow during that year; therefore, this amount is subtracted from the 1973-74 Base Flow.

Base Flow

Unlike previous years, the determination of the Base Flow curve was complicated by the significant quantities of State water which was released upstream of Prado Dam during 1972-73 and 1973-74. As in previous years, the release of stored Storm Flow over extended periods also masked the magnitude of the Base Flow during non-storm periods.

The general procedure used by the members of the Watermaster to separate the 1973-74 flow components is outlined below:

- (1) The daily records at Prado Dam, as measured by the USGS, were plotted for the entire water year as shown on Plate 2.
- (2) To facilitate the separation of the Storm Flow component from the Base Flow component, the daily inflow to Prado Reservoir was estimated. This was done by using reservoir stage records secured from the Corps of Engineers and the daily outflows as measured by the USGS. Daily reservoir water surface elevations were converted to acre-feet of storage by use of Corps of Engineers' relationships between the water surface elevation and the storage capacity. Daily reservoir inflow was computed by use of the equation: Inflow = Outflow + Change in Reservoir Storage.
- (3) The daily flow component due to the release of State water into San Antonio Creek during 1973-74 was estimated and subtracted from the daily inflows as determined in Item (2) above.

The Watermaster identified probable losses of State water due to seepage in the Rialto Feeder and the seepage and evapo-transpiration losses in the lined and unlined channels and in Prado Reservoir.

The estimated delivery of State Project water was based on State of California, Department of Water Resources' weekly meter charts and daily meter readings of the Nontributary water released at Devil Canyon. Travel time delays for the several reaches between Devil Canyon and

Prado were estimated. These estimates of delays, which are to be restudied, affect the shape and positioning of the Base Flow curve.

After independently examining these factors, the Watermaster agreed to use a loss of 3.14% of the amount of water released. They also agreed to make subsequent investigations to better define the losses associated with these State Project water releases and to make adjustments in the 1973-74 State Project water flow at Prado, if future investigations indicate that the actual losses are materially different from those used in the 1973-74 computations.

These losses were distributed in accordance with the above stated procedure on a daily basis. The resultant Nontributary water reaching Prado amounted to 63,035 acre-feet. The estimated daily inflows to Prado reduced by the amount of said Nontributary flow were plotted for the entire water year as shown on Plate 2.

- (4) The daily precipitation recorded at the San Bernardino County Hospital is shown on Plate 2.
- (5) Using the above data, an initial determination was made of those days having no Storm Flow component when there were no sharp peaks in the hydrograph. Non-storm periods exclude the time from commencement of rainfall until the end of the recession flow following each storm period. Use was made of the inflow hydrograph to determine Base Flow when discharge of stored water occurred during non-storm periods. All adjacent non-storm days were fitted with smooth curve segments to average out the day-to-day fluctuations.
- (6) Utilizing the above curve segments during non-storm periods, a continuous smooth Base Flow curve was drawn and extended across the balance of the time when storms occurred. The shape of the curve throughout the year is generally similar to those of prior years, except for the exaggeration of the Base Flow Curve as previously discussed. During periods of Storm Flow when changes in storage occurred in Prado reservoir, the inflow hydrograph was used as a guide.
- (7) Arriving at an opinion of the location of the curve separating the two components of flow required the exercise of judgment, taking into consideration items (1) through (6) above and, to some extent, the variation in Base Flow which occurred in the previous water year.
- (8) The Base Flow curve is used for separation of components of flow during storm intervals. Mean daily Storm Flow was computed by subtracting the value of the Base Flow curve from the computed total mean daily inflow. For these days, Base Flow was designated as the value shown on the Base Flow Curve.

- (9) In addition to the State Water project flows at Prado, which were determined in item (3) above, the State Project water releases during 1972-73 increased the flows due to rising water from the Riverside groundwater basin. Of the total State Project water released into Santa Ana River upstream of Riverside Narrows during water year 1972-73, 473 acre-feet were delivered through Prado Dam and 11,140 acre-feet remained in groundwater storage at the end of that water year. The members of the Watermaster agreed that 980 acre-feet of the 11,140 acre-feet arrived at Prado during 1973-74. They also agreed that 20 acre-feet were lost due to evapo-transpiration and 10,140 acre-feet remained in groundwater storage on September 30, 1974. It was also agreed that these amounts could be modified if warranted by the investigation to be conducted during the coming year.
- (10) For those days outside the storm periods, Base Flow was accepted as the computed inflow less the Nontributary flows.

Water Quality

During the water year 1973-74, the weighted average total dissolved solids (TDS) for the total flow, including Nontributary flow, passing Prado was found to be 462 ppm. This determination of the water quality at the USGS gaging station below Prado Dam was made using measurements obtained by the USGS which operates a water quality monitoring recorder at this station. A continuous stream of water from the Santa Ana River is pumped to the water quality monitor. A continuous record of data recorded on a punched tape is obtained for determination of specific conductivity and temperature. Average daily values for TDS which were generated from specific conductance data recorded at this water quality station are shown on Plate 3.

The plot of TDS on Plate 3 shows the effects of the State Project water. In general, the TDS fluctuated in the 300 to 500 ppm range when the State Project water was being released. During April when the release of State Project water was reduced to 50 cfs, there was a corresponding increase in TDS to the 500 to 600 ppm range. During periods when State Project water was not being released, the TDS generally fluctuated in the 700 to 800 ppm.

Personnel from the USGS make weekly inspections of the station to determine if equipment is operating satisfactorily and to secure grab samples of water from the river for laboratory determinations of total dissolved solids and for specific conductance. During periods of storm runoff the USGS visits the station at least once each day for the purpose of taking additional grab samples to provide a more detailed record of possible changes in water quality during periods of Storm Flow. These samples are analyzed for TDS and for specific conductance.

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At the end of each month, the punched tape from the Prado monitoring unit is transmitted to Washington, D.C. for machine processing. A summary tabulation of data for all items is obtained. The summary also shows the maximum, minimum and the mean hourly reading each day of record. The results of the machine processing are returned to the USGS staff in Garden Grove, California for review and to eliminate inconsistent data. A corrected summary is then made available to the Watermaster, along with a more detailed record of specific conductances showing instantaneous values at two-hour intervals.

Utilizing the USGS water quality records, the following analyses were performed by the Watermaster to determine the annual weighted TDS:

- (1) The specific conductivity of the Santa Ana River below Prado was relatively uniform for most days of the year. On these days, the mean hourly specific conductance, as computed by the USGS, was accepted as representative of the daily weighted value.
- (2) During periods when the daily discharge varied, numerous flow measurements, together with the respective specific conductance measurement, were used to determine the weighted mean daily specific conductance value.
- (3) Laboratory analyses of the 43 grab samples taken by the USGS below Prado Dam during the 1973-74 season were run to determine both specific conductance and TDS. Results of these analyses were used to prepare a correlation between specific conductance and the corresponding TDS. A detailed discussion of this statistical analysis is presented in the following section.
- (4) The resulting equation from the curve fitting operation was then used to determine the mean daily TDS corresponding to the mean daily specific conductance values for each day of the year.
- (5) The mean daily TDS values were then multiplied by the mean daily flow. These products were then summed and divided by the total flow for the year to determine the weighted average TDS value for the water year. This value for TDS for the total flow including Nontributary water was 462 ppm of total dissolved solids for the 1973-74 water year. This value hereinafter is adjusted for the quality of the Nontributary flow.

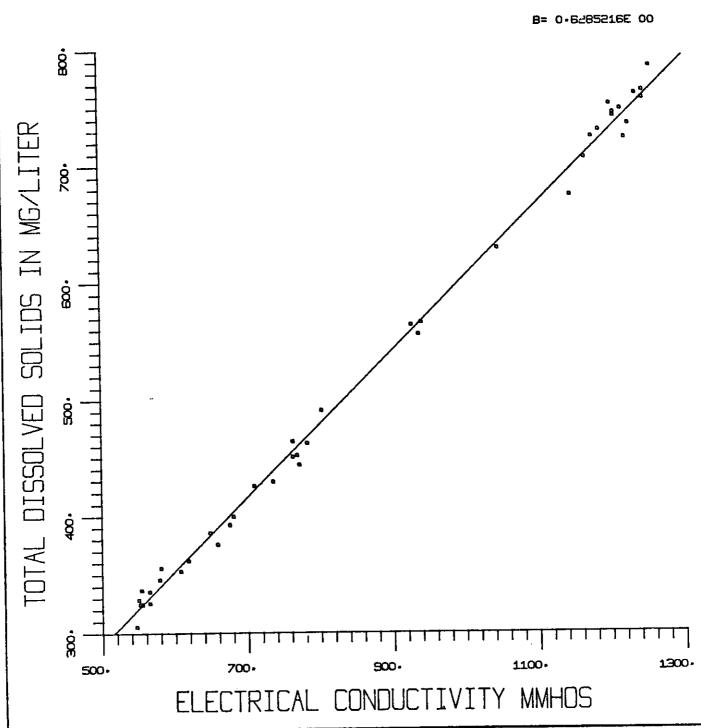
Statistical Analysis of EC and TDS Relationships

An analysis of the correlation of electrical conductivity versus total dissolved solids in the Santa Ana River below Prado Dam for the water year 1973-74 was analyzed through the use of a

TDS AS A FUNCTION OF E.C. BELOW PRADO DAM

Y=A+B+X

A=-0.2384645E 02



statistical computer program. This is a linear regression program for data sets in two variables; x and y. From input data points, described by their x and y coordinates, an equation is produced that best fits these points from a least squares viewpoint. The computer program calculates six different types of equations based on the assumption that y (TDS) is a function of the independent variable x (EC). The computer output results of the analysis of the 1973-74 data is shown below.

Form of Equation	Curve Type	Correlation Coefficient	Y- Intercept (A)	Slope (B)
(1) TDS=A+B (EC)	Linear Exponential Power Function Hyperbolic Hyperbolic Hyperbolic	0.9948	-23.85	0.6285
(2) TDS=A[EXP (BxEC)]		0.9891	175.79	11.92x10 ⁻⁴
(3) TDS=A (EC)B		0.9939	0.4409	1.045
(4) TDS=A+B/EC		0.9734	1084.4	-44.43x10 ⁻⁴
(5) TDS=1/[A+B (EC)]		0.9713	41.92x10 ⁻⁴	-23.79x10 ⁻⁷
(6) TDS=EC/[A+B (EC)]		0.9909	1.753	-92.07x10 ⁻⁶

Note that the value of the correlation coefficient for equation (1) most nearly approaches 1.000-the value which represents a perfect correlation between x and y data points. On the basis of these statistics, equation (1) was selected as the relationship for relating the 1973-74 USGS mean daily electrical conductivity values to mean daily TDS values. The equation, as shown on Figure 4, used for this relationship was:

$$TDS = -23.85 + (0.6285)$$
 (EC)

Water Quality Adjustment for Nontributary Water

The weighted average annual TDS value of 462 ppm, as stated previously, includes the effects of the State Project water during this water year and the preceding water year. The value also includes the effects of 1,109 acre-feet of 1972-73 Base Flow released in 1973-74 water year. Therefore, the volumes of water and the amounts of salts contributed by these releases were subtracted from the quantities which determine the TDS value. The flow-weighted average TDS of the State Project water released at Devil Canyon during water year 1973-74 was 218 ppm. The flow-weighted average TDS of State water released during 1972-73 was 235 ppm. The average TDS of the 1972-73 Base Flow released during 1973-74 was 729 ppm. After adjusting for these releases, the weighted average annual TDS value for 1973-74 is 704 ppm. The basic information used in the statistical analysis is included herein as Appendix D.

Adjusted Base Flow

According to the Judgment, "The amount of Base Flow at Prado received during any year shall be subjected to adjustment based on weighted average annual TDS in Base Flow and Storm Flow at Prado as follows:

If the Weighted Average TDS in Base Flow and Storm Flow at Prado is:	Then the Adjusted Base Flow shall be determined by the formula:		
Greater than 800 ppm	$Q = \frac{35}{42,000} Q \text{ (TDS-800)}$		
700 ppm - 800 ppm	Q		
Less than 700 ppm	$Q + \frac{35}{42,000} Q (700-TDS)$		

Where: Q=Base Flow actually received."

As noted previously, the Base Flow of the Santa Ana River below Prado Dam determined by the Watermaster amounted to 43,769 acre-feet for water year 1973-74. The weighted average annual TDS of the total flow is 704 ppm. No adjustment to the Base Flow of 43,769 acre-feet is necessary because the value of the weighted average annual TDS lies between 700 and 800 ppm.

Entitlement and Credit or Debit

From pages 12 and 13 of the Judgment, the following description of the obligation of the CBMWD and WMWD is given: "CBMWD and WMWD shall be responsible for an average annual adjusted Base Flow of 42,000 acre-feet at Prado....CBMWD and WMWD each year shall be responsible for not less than 37,000 acre-feet of Base Flow at Prado, plus one-third of any cumulative debit..."

The Watermaster is required to maintain a continuing account of a list of permanent items at Prado for each year. A list of these items and the 1973-74 values are shown below:

43,769 acre-feet	Base Flow at Prado	(1)
704 ppm	Annual Weighted TDS of Total Flow	(2)
43,769 acre-feet	Annual Adjusted Base Flow	(3)
174,118 acre-feet	Cumulative Adjusted Base Flow	(4)
168,000 acre-feet	Cumulative Entitlement of OCWD at Prado	(5)
6,118 acre-feet	Cumulative Credit (4)-(5)	(6)
0 acre-feet	One-Third of Cumulative Debit	(7)
37,000 acre-feet	Minimum Required Base Flow in 1974-75	(8)



Nontributary State Project water and Base Flow flowing in outlet channel downstream of Prado Dam

CHAPTER V

BASE FLOW AT RIVERSIDE NARROWS

The Judgment states that SBVMWD is "responsible for an average annual Adjusted Base Flow of 15,250 acre-feet at Riverside Narrows". This chapter deals with the analysis of the flow at Riverside Narrows, the calculation of the amount of Base Flow received and credited to SBVMWD, and the calculation of the amount of Base Flow received and credited to SBVMWD, and the calculation of the Adjusted Base Flow, the adjustment being made on the basis of the weighted average annual TDS in the Base Flow.

Total Discharge at Riverside Narrows

The surface flow of the river at the Riverside Narrows has been measured by the USGS since 1929, first at a gaging station located approximately one-half mile downstream from the Union Pacific Railroad Bridge, which was moved in 1943 to a downstream location at Pedley crossing, now known as Van Buren Boulevard. A flood which occurred during the 1968-69 water year washed out a portion of the bridge across the river at this location. This increased the difficulty of maintaining the surface gage at Van Buren Boulevard, and led to the installation of a surface water gaging station upstream a short distance above The Metropolitan Water District Upper Feeder Bridge crossing which is situated on the opposite side of the river from the original location of the Riverside Narrows surface water gaging station. This surface water gaging station, which is $1\frac{1}{2}$ miles upstream from Van Buren Boulevard, also houses a monitor for the determination of electrical conductivity.

In 1947, the City of Riverside constructed a sewage treatment plant a short distance upstream from Van Buren Boulevard. This plant was enlarged in 1968 and the effluent was discharged directly to the Santa Ana River upstream from Van Buren Boulevard, with the result that the surface water flow at Van Buren Boulevard includes the sewage effluent from the Riverside Water Quality Control Plant.

For the year of 1971-72, the Base Flow component was calculated at the two gaging stations, one at Van Buren Boulevard and the other at the MWD Upper Feeder crossing. The Base Flow, as calculated at the Upper Feeder crossing, was found to be slightly higher than that calculated at Van Buren Boulevard, and for the year of 1971-72 it was the Watermaster's decision that the Base Flow at the Riverside Narrows would be defined as that portion of the total surface flow passing the

gaging station at Van Buren Boulevard which remained after the deduction of Storm Flow and the wastewater discharge to the river by the City of Riverside above the measuring plant.

Dual measurements were continued during the year of 1972-73 through June of 1973, at which time the USGS discontinued measurements at the Van Buren Boulevard gaging station. The surface water gaging station just upstream of the MWD Upper Feeder Bridge crossing has been used as the source of flow data for the 1973-74 water year.

Nontributary Flow

During the period May through September 1973, Nontributary water from the East Branch of the California Aqueduct was released into the Santa Ana River in the vicinity of Colton. This release was made at the request of the Orange County Water District and totaled 11,617 acre-feet. This water percolated into the Riverside Basin and for the water year 1972-73, the Watermaster reached the conclusion that as of September 30, 1973, 477 acre-feet had passed Riverside Narrows.

At the beginning of the 1973-74 water year, the remaining 11,140 acre-feet of Nontributary water existed as water in storage in the Riverside Basin, moving toward the Riverside Narrows where either all or part of it will appear as rising water. Because of the nature of its movement, it is impossible to distinguish this Nontributary water from normal Base Flow by means of scalping procedures used by the Watermaster. During the past year some indication of the amount of this Nontributary water reaching Riverside Narrows could be derived from a water quality study (the Nontributary water is of better quality from a total dissolved solids point-of-view than normal Base Flow), but even this type of distinction will be completely masked in a short period of time.

Accordingly, the Orange County Water District conducted a detailed mathematical analysis of the recharge operation based on the Dupuit-Forcheimer approximations to Darcy's Law for flow through porous media. An analysis of this nature working with as complex a system as an alluvium-formed aquifer must incorporate many simplifying assumptions so that the resulting equations can be solved. This has been accomplished in a preliminary form, and the Watermaster is in the process of reviewing the results. Due to the time factor, however, in developing a Base Flow value by February for this water year, 1973-74, the Watermaster has accepted, on a tentative basis, the results of the mathematical analysis for the year 1973-74, and has adjusted it to a rounded-off value of 1,000 acre-feet. During the coming year, (74-75), the Watermaster will attempt to conclude its analysis and negotiation on this Nontributary water and develop a statement on how it should be handled in future years. The Watermaster has agreed that the value of 477 acre-feet and 1,000

acre-feet for the water years 1972-73 and 1973-74, respectively, may be modified and such modifications incorporated in next year's findings, if the agreed-upon solution indicates that such modifications are warranted.

Components of Flow

The components of the total flow of the Santa Ana River at Riverside Narrows at MWD Crossing for the 1973-1974 water year include Nontributary, Storm and Base Flow. These components, by months, as listed on Table 5, represent an average value derived from calculations made by the five members of the Watermaster.

TABLE 5

COMPONENTS OF FLOW AT RIVERSIDE NARROWS FOR WATER YEAR 1973-74
(Quantities in Acre-Feet)

	Month	Total Flow USGS Measurement	Nontributary Flow	Storm Flow	Base Flow
1973	October	1,258	83	0	1,175
	November	1,718	83	443	1,192
	December	1,434	83	12	1,339
1974	January	8,083	83	6,535	1,465
	February	1,831	83	28	1,720
	March	3,078	83	1,148	1,847
	April	1,749	83	125	1,541
	May	1,660	83	0	1,577
	June	1,297	84	0	1,213
	July	1,190	84	0	1,106
	August	1,123	84	0	1,039
	September	1,073	84	0	989
Total	- Acre Feet	25,494	1,000	8,291	16,203

The total flow, as shown in Table 5, consists of 3.92% of Nontributary Flow, 32.52% Storm Flow, and 63.56% Base Flow.

Base Flow

The hydrograph of the river flow at the MWD Crossing shows the scalped Storm Flow component colored in red on Plate 4. Based on this hydrograph and utilizing in general the same procedures as are reflected in the Work Papers of the engineers (as referenced in Paragraph 2 of the Engineering Appendix of the Judgment), a separation was made between Storm Flow and the sum of Base Flow and Nontributary water and the two components calculated. Nontributary water was assumed to be equally distributed throughout the year (1,000 acre-feet divided by 12 months) and subtracted from the sum of the Base Flow and Nontributary water to arrive at Base Flow.

Each of the five members of the Watermaster independently made a determination of each component, based on his own judgment and his own interpretation of the method used in the previously referenced Work Papers. The value for Base Flow of 16,203 acre-feet, as shown on Table 5 is the mathematical average of the five determinations. Plate 4 is indicative of the scalping done by the Watermaster.

Water Quality

Under the terms of the Judgment it is necessary to determine the weighted average total dissolved solids (TDS) content of the Base Flow at Riverside Narrows.

To accomplish this, the USGS has installed a specific conductance measuring device and recorder immediately upstream from the river crossing of the Upper Feeder of MWD, which is also upstream from the point of discharge of the effluent from the Riverside Water Quality Control Plant to the river. The USGS operates and maintains this monitoring device in the same manner as the station operated at below Prado Dam. The data collected from this monitor are augmented by periodic grab samples.

During the water year 1973-74, 50 samples were taken from the waters of the Santa Ana River at the MWD Crossing for laboratory analysis, to determine the TDS and EC of each sample. All 50 samples were used in a statistical analysis for the determination of the relationship of EC to TDS. Appendix E includes the complete statistical analysis.

Statistical Analysis of EC and TDS Relationships

Six different types of equations were utilized, based upon the assumption that TDS was a function of the independent variable EC, to determine the equation providing the best correlation. The analysis was made utilizing a multiple regression computer program which determined the best curve fitting equation for the 50 laboratory samples.

The results of the computer analysis of the 1973-74 data are shown as follows:

Form of Equation	Curve Type	Multiple Correlation Coefficient	Coefficient Term (A)	Constant Term (B)
(1) TDS = A(EC) + B	Linear	0.974	0.6230	0.1546
(2) TDS = $A[ln(EC)] + B$	Logarithmic	0.964	386.3280	-2021.8222
(3) TDS = $\frac{1.0}{A \text{ (EC) +B}}$	Hyperbolic	0.982	-4.529 x 10 ⁻⁶	6.421 x 10 ⁻³
$(4) TDS = A [e^{B(EC)}]$	Exponential	0.986	123.06344	0.00156
(5) TDS = $\frac{EC}{A(EC) + B}$	Hyperbolic	0.997	5.1×10^{-5}	1.54979
(6) TDS = $A (EC)^B$	Exponential	0.991	0.68777	0.9858

Note that the value of the multiple correlation coefficient for equation (5) most nearly approaches 1.0000 - the value which represents a perfect correlation between the TDS and EC samples. Based on the above computer analysis, equation (5) was selected as the relationship for relating the 1973-74 mean daily electrical conductivity values to the adjusted daily TDS values. The equation used for this relationship was:

$$TDS = \frac{EC}{0.000051(EC) + 1.54979}$$

The adjusted daily TDS calculated by the above equation was then multiplied by the mean daily flow for each day of the year as shown on Table No. E-2, Appendix E, entitled "Weighted T.D.S. Calculation Sheet".

Because the Judgment provides that only the base flow at the Riverside Narrows may be used for determining the weighted average annual TDS, the calculation sheets separate the total flow into two parts, the Storm Flow and the sum of Nontributary and Base Flow. The two components used were those developed by Mr. Albert A. Webb, because he was responsible for this particular

calculation of the weighted water quality. The monthly totals of the product of the adjusted TDS and the three flows (Total, Storm, and Nontributary + Base) were calculated for each month.

The adjusted TDS during Storm Flows were corrected averaging the TDS on the day before and the day after the storm as shown on Table No. E-2 of Appendix E. The corrected TDS were then multiplied by the Nontributary and Base Flow component only, and has been noted by one asterisk on the calculation sheets on said Table No. E-2.

The calculation sheets on said Table No. E-2 have been summarized on Table No. E-3 of Appendix E, entitled "Summary of Water Quality for the Riverside Narrows at Metropolitan Water District (MWD) Crossing". The weighted average annual total dissolved solids in parts per million (ppm) of the Santa Ana River at MWD crossing for water year 1973-74, for the Nontributary and Base Flow component was 674 ppm. To adjust this for Base Flow only, it was assumed that the Nontributary water had an original quality of 235 ppm. The adjustment for the Nontributary water results in a TDS for Base Flow only of 700 ppm.

A plot of the TDS of the total daily flow, including Nontributary water, at the MWD Crossing for the water year 1973-74 is shown on Plate 5, together with the San Bernardino rainfall.

Adjusted Base Flow at Riverside Narrows

The Judgment provides that the amount of Base Flow at Riverside Narrows received during any year shall be subject to adjustment based on the weighted average annual TDS in such Base Flow as follows:

If the Weighted Average TDS in Base Flow at Riverside Narrows is:	Then the Adjusted Base Flow shall be Determined by the Formula:
Riverside Trainer	
Greater than 700 ppm	$Q - \frac{11}{15,250} Q \text{ (TDS-700)}$
600 ppm - 700 ppm	Q
Less than 600 ppm	$Q + \frac{11}{15,250} Q (600-TDS)$

Where Q = Base Flow actually received.

From the previous subsection, the weighted average annual TDS in the Base Flow at Riverside Narrows for the water year 1973-74 was 700 ppm. Therefore, no adjustment to the Base Flow of 16,203 acre-feet was necessary because the value of the weighted average annual TDS was not greater than 700 ppm.

Entitlement and Credit or Debit

Paragraph 5(b) of the Judgment states that "SBVMWD shall be responsible for an average annual Adjusted Base Flow of 15,250 acre-feet at Riverside Narrows.....SBVMWD each year shall be responsible at Riverside Narrows for not less than 13,420 acre-feet of Base Flow plus one-third of any cumulative debit...."

A list of the accounting items and the 1973-74 values for these items, as required by Paragraph 4 of the Engineering Appendix to the Judgment, is detailed below:

(1)	Base Flow at Riverside Narrows	16,203 acre-feet
(2)	Annual Weighted TDS of Base Flow at Riverside Narrows	700 ppm
(3)	Annual Adjusted Base Flow	16,203 acre-feet
(4)	Cumulative Adjusted Base Flow	66,337 acre-feet
(5)	Cumulative Entitlement of CBMWD and WMWD	
	at Riverside Narrows	61,000 acre-feet
(6)	Cumulative Credit (4)-(5)	5,337 acre-feet
(7)	One-third of Cumulative Debit	0
(8)	Minimum Required Base Flow in 1973-74	13,420 acre-feet

APPENDIX A

HISTORY OF LITIGATION

HISTORY OF LITIGATION

The complaint in this case was filed by the Orange County Water District on October 18, 1963 seeking an adjudication of water rights against more than 2,500 water users in the area tributary to Prado Dam within the Santa Ana River Watershed. Thirteen cross-complaints were filed in 1968 extending the adjudication to include an additional 1,500 water users in the area downstream from Prado Dam. Thus, there were involved in this case some 4,000 parties. It became obvious that every effort should be made to arrive at a settlement and a physical solution in order to avoid the enormous and unwieldy litigation that would be involved.

Efforts to arrive at a settlement and physical solution were pursued by public officials, individuals, attorneys, and engineers. Attorneys for the parties organized in order to further this objective. Among other things, they provided guidance for the formation and activities of an engineering committee to provide them with information on the physical facts.

An initial meeting of the engineers representing the parties was held on January 10, 1964. Agreement was reached that it would be beneficial to jointly undertake the compilation of basic data. Liaison was established with the Department of Water Resources, State of California, on requests for information to be obtained from the State's studies for use by the parties. Engineers representing the parties were divided into sub-committees which were given the responsibility of investigating such things as the boundary of the Santa Ana River watershed and its subareas, standardization of the terminology, the location and description of wells and diversion facilities, waste disposal and transfers of water between subareas.

On April 30, 1964, the joint engineering committee prepared a list of preliminary engineering studies directed toward settlement of the Santa Ana River water rights litigation. This list of basic information was in response to a request from the attorneys' committee at a meeting held April 17, 1964. Special assignments were made on selected items to individual engineers to provide information requested by the attorneys' committee.

The attorneys and engineers for the defendants then commenced a series of meetings separate from the representatives of the plaintiff in order to consolidate their position and to determine their course of action. On October 7, 1964 engineers for the defendants presented the results of the studies made by the joint engineering committee. The defendants' attorneys requested that additional information be provided on the methods of measuring flow at Prado and the historical supply and disposal of water passing Prado Dam segregated into the components of flow and

designating the amount of supply which was usable by the downstream area. On December 11, 1964, this supplemental information was presented to the defendants' attorneys.

During 1965, engineers and attorneys for the defendants held numerous conferences and conducted additional studies in an attempt to determine their respective positions in the case. Early in 1966, the plaintiff and defendants exchanged drafts of possible principles of settlement. Commencing March 22 and ending April 13, 1966, four meetings were held by the engineers to discuss the draft of principles for settlement.

On February 25, 1968 the defendants submitted a request to the Court that an Order of Reference be issued requesting the State Department of Water Resources to determine the physical facts. On May 9, 1968 the plaintiff's attorney submitted motions opposing the Order of Reference and requesting that a preliminary injunction be issued. In the meantime, every effort was being made to come to an agreement on a stipulated judgment. Commencing on February 28, 1968 and extending until May 14, 1968, six meetings were held to determine the scope of physical facts on which agreement could be reached so that if an Order of Reference were to be approved by the Court, the work under the proposed reference would not repeat the extensive basic data collection and compilation which had already been completed and on which engineers for both plaintiffs and defendants had reached substantial agreement. Such basic data were compiled and published in two volumes under date of May 14, 1968 entitled "Appendix A. Basic Data."

On May 21, 1968 an outline of a proposal for settlement of the case was prepared and a committee of attorneys and engineers for the parties commenced preparation of the settlement documents. On June 16, 1968, the Court held a hearing on the motions it had received requesting a preliminary injunction and an Order of Reference. The parties requested that the Court delay the hearings on these motions in view of the efforts toward settlement that were underway. The plaintiff, however, was concerned regarding the necessity of bringing the case to trial within the statutory limitation and, accordingly, on July 15, 1968 submitted a motion to set the complaint in the case for trial. On October 15, 1968 the trial was commenced and was adjourned after one-half day of testimony on behalf of the plaintiff. Thereafter, the parties filed with the Court the necessary Settlements Documents including a Stipulation for Judgment. The Court entered the Judgment on April 17, 1969. This terminated the many years of controversy over water rights along the Santa Ana River involving the issues and parties embraced in Orange County Water District versus City of Chino, et al.

APPENDIX B

SUMMARY OF JUDGMENT

SUMMARY OF JUDGMENT

Provisions of the Judgment became effective on October 1, 1970. The Judgment does not define the water rights of the individual claimants. Instead, it provides for a regional allocation of water supply of the Santa Ana River system and establishes entitlements and obligations among the four existing major public water districts overlying the aggregate of substantially all of the major areas of water use in the watershed. Dismissals were entered as to all defendants and cross defendants other than these four major public districts. These districts, the locations of which are shown on Plate 1, "Santa Ana River Watershed," are the remaining parties to the Judgment and are as follows:

- (1) Orange County Water District (OCWD), representing all lower basin entities which are located within Orange County downstream from Prado Dam.
- (2) Western Municipal Water District (WMWD), representing middle basin entities located within Riverside County on both sides of the Santa Ana River primarily upstream from Prado Dam.
- (3) Chino Basin Municipal Water District (CBMWD), located in San Bernardino County Chino Basin area, representing middle basin entities within its boundaries and located primarily upstream from Prado Dam.
- (4) San Bernardino Valley Municipal Water District (SBVMWD), representing all entities within its boundaries, and embraced within the upper portion of the Riverside Basin Area, the Colton Basin area (being an upstream portion of the middle basin) and the San Bernardino Basin area, being essentially the upper basin.

A physical solution under the stipulated Judgment provides, in general, that SBVMWD shall be responsible for the delivery of an average annual amount of Base Flow at Riverside Narrows and CBMWD and WMWD shall jointly be responsible for an average annual amount of Base Flow at Prado. Essential to the understanding of the provisions of the Judgment is the definition of certain important terms. The total surface flow passing a point of measurement is divided into components, which are defined in the Judgment as follows:

"(1) Storm Flow - That portion of the total surface flow passing a point of measurement, which originates from precipitation and runoff without having first percolated to ground water storage in the zone of saturation, calculated in accordance with procedures referred to in Exhibit B.

- (2) Base Flow That portion of the total surface flow passing a point of measurement which remains after deduction of storm flow.
- (3) Adjusted Base Flow Actual base flow in each year adjusted for quality as provided . . ."

The Judgment sets forth a declaration of rights. Briefly stated, the Judgment provides that the water users in the area downstream from Prado Dam have rights, as against the upstream users, to receive an average annual supply of 42,000 acre-feet of Base Flow at Prado Dam, together with the right to all Storm Flow reaching Prado Dam. Water users in the area upstream of Prado Dam, as against the downstream users, have the right to divert, pump, extract, conserve, store and use all surface and ground water supplies originating within the upper area, so long as the lower area receives the water to which it is entitled.

The physical solution set forth in the Judgment requires that SBVMWD shall be responsible for an average annual Adjusted Base Flow of 15,250 acre-feet at Riverside Narrows subject each year to the following:

- (1) A minimum Base Flow of 13,420 acre-feet plus one-third of any cumulated debit.
- (2) After October 2, 1986, if no cumulated debit exists, the minimum quantity shall be 12,420 acre-feet.
- (3) Prior to 1986, if the cumulated credit exceeds 10,000 acre-feet the minimum quantity shall be 12,420 acre-feet.
- (4) All cumulated debits shall be removed by the discharge of a sufficient Base Flow at Riverside Narrows at least once in every ten consecutive years following October 1, 1976. Any accumulated credits shall remain on the books of account until used to offset any subsequent debits or until otherwise disposed of by SBVMWD.
- (5) The Base Flow at Riverside Narrows shall be adjusted using weighted average annual TDS in such Base Flow in accordance with the formula set forth in the Judgment.

The obligations under the physical solutions for meeting the Adjusted Base Flow of 42,000 acre-feet at Prado Dam for the benefit of the downstream water users as shared by CBMWD and WMWD are as follows:

- (1) Minimum Base Flow at Prado shall not be less than 37,000 acre-feet plus one-third of any cumulated debit.
- (2) After October 1, 1986, if no cumulated debit exists, the minimum quantity shall be 34,000 acre-feet.
- (3) Prior to 1986, if the cumulated credit exceeds 30,000 acre-feet, the minimum quantity shall be 34,000 acre-feet.

- (4) Sufficient quantities of Base Flow shall be provided at Prado to discharge completely any cumulated debits at least once in any ten consecutive years following October 1, 1976. Any cumulative credits shall remain on the books of account until used to offset any subsequent debits, or until otherwise disposed of by CBMWD and WMWD.
- (5) The Base Flow at Prado during any year shall be adjusted using the weighted average annual TDS in the total flow at Prado (Base Flow plus Storm Flow) in accordance with the formula set forth in the Judgment.

The accounting provided for under the Judgment allows credit to be earned when the average annual Adjusted Base Flow exceeds 15,250 acre-feet at Riverside Narrows and 42,000 acre-feet at Prado. Debits accrue when the average annual Adjusted Base Flow falls below the above quantities at the respective locations. The adjustment of Base Flow for water quality is to provide an incentive to maintain a better quality water as a result of implementation of the physical solution. That is, when the water quality is improved over a certain amount, the quantitative amount of the obligation is decreased; but when that water quality is impaired beyond a specified limit, the quantity of the obligation is increased. This is one of the first comprehensive adjudications in Southern California which includes provisions applicable to the quality of water in addition to the determination of quantitative rights.

APPENDIX C

NONTRIBUTARY WATER DELIVERED TO ORANGE COUNTY WATER DIS-TRICT BY MWD FROM THE RIALTO FEEDER TO SAN ANTONIO WASH NEAR MONTCLAIR (CONNECTION OC59-T)

1973-74

Prepared By

Albert A. Webb

SUMMARY

OF

NONTRIBUTARY WATER RELEASED AT OC-59T FROM DEVIL CANYON POWERPLANT AFTERBAY TO M.W.D. RIALTO PIPELINE WATER YEAR 1973-74

Month	Acre Feet
October	0
November	0
December	7,402
January	2,623
February	7,337
March	1,529
April	3, 127
May	5,505
June	7,761
July	11,469
August	12, 128
September	6,197
Total	65,078

December, 1973

					Total From	
	36" Meter		90" Meter		36" & 90" Meters	
Day	A.F.	cfs	A.F.	cfs	A.F.	cfs_
1	0	0	0	0	0	0
2	0	0	0	0	0	0
3	43.01	21.7	0	0	43.01	21.7
4	101.55	51.2	0	0	101.55	51.2
5	34.63	17.5	152.64	77.0	187.27	94.5
6	0	0	198.38	100.0	198.38	100.0
7	0	0	249.60	125.8	249.60	125.8
8	0	0	272.70	137.5	272.70	137.5
9	0	0	360.37	181.7	360.37	181.7
10	0	0	395.21	199.3	395.21	199.3
11	0	0	392.19	197.7	392.19	197.7
12	0	0	391.63	19 7. 5	391.63	197.5
13	0	0	363.23	183.1	363.23	183.1
14	0	0	281.21	141.8	281.21	141.8
15	0	0	0	0	0	0
16	0	0	0	0	0	0
17	0	0	0	0	0	0
18	0	0	0	0	0	0
19	0	0	0	0	0	0
20	0	0	0	0	0	0
21	3.63	1.8	244.81	123.4	248.44	125.2
22	0	0	391.75	197.5	391.75	197.5
23	0	0	391.75	197.5	391 .7 5	197.5
24	0	0	391.7 5	197.5	391.75	197.5
25	0	0	391.75	197.5	391.75	197.5
26	0	0	391.75	197.5	391.75	197.5
27	0	0	391.75	197.5	391.75	197.5
28	0	0	391.75	197.5	391.75	197.5
29	0	0	391.76	197.5	391.76	197.5
30	0	0	391.76	197.5	391.76	197.5
31	0	0	391.7 6	197.5	391.7 6	197.5
Total	182.82	92.2	7,219.50	3,639.8	7,402.32	3,732.0

NONTRIBUTARY WATER FROM DEVIL CANYON POWERPLANT AFTERBAY (OC-59T) AS DISCHARGED TO M. W.D. RIALTO PIPELINE

FROM 36" AND 90" VENTURI METERS

January, 1974

			Danuary,	1/11			
					Total F		
	36" M		90" M		36" & 90":		
Day	A.F.	cfs	A.F.	cfs	A.F.	cfs	
_	•	0	201 75	107 5	391.75	197.5	
1	0	0	391.75	197.5			
2	0	0	391.75	197.5	391.75	197.5	
3	0	0	391.76	197.5	391.76	197.5	
4	0	0	167.68	84.5	167.68	84.5	
5	0	0	0	0	0	0	
6	0	0	0	0	0	0	
7	0	0	0	0	0	0	
8	0	0	0	0	0	0	
9	0	0	0	0	0	0	
10	0	0	0	0	0	0	
11	0	0	0	0	0	0	
12	0	0	0	0	0	0	
13	0	0	0	0	0	0	
14	0	0	0	0	0	0	
15	0	0	0	0	0	0	
16	0	0	0	0	0	0	
17	0	0	0	0	0	0	
18	0	0	0	0	0	0	
19	0	0	0	0	0	0	
20	0	0	.0	0	0	0	
21	0	0	0	0	0	0	
22	0	0	0	0	0	0	
23	0	0	0	0	0	0	
24	0	0	0	0	0	0	
25	0	0	0	0	0	0	
26	0	0	0	0	0	0	
27	0	0	0	0	0	0	
28	0	0	256.68	129.4	256.68	129.4	
29	0	0	396.46	199.9	396.46	199.9	
30	0	0	383.40	193.3	383.40	193.3	
31	0	0	243.76	122.9	243.76	122.9	
Total	0	0	2,623.24	1,322.5	2,623,24	1,322.5	

February, 1974

						Total From	
	36" Meter		90'' M	90" Meter		Meters	
Day	<u>A.F.</u>	cfs	A.F.	cfs	A.F.	cfs	
1	0	0	0	0	0	0	
1 2	0	0	0	0	0	0	
3	0	0	0	0	0	0	
3 4	0	0	0	0	0	0	
5	0	0	260.12	131.1	260.12	131.1	
		0	499.43	251.8	499.43	251.8	
6	0	0			503.33	251.8	
7	0		503.33	253.8			
8	0	0	372.64	187.9	372.64 305.63	187.9	
9	0	0	305.63	154. l		154.1	
10	0	0 0	305.63	154.1 154.1	305.63 305.63	154.1 154.1	
11	0		305.63		305.63	154.1	
12	0	0	305.63	154.1			
13	0	0	305.63	154.1	305.63	154.1	
14	0	0	305.63	154.1	305.63	154.1	
15	0	0 0	305.63	154.1	305.63	154.1	
16	0		214.29	108.0	214.29	108.0	
17	5.85	3.0	112.94	56.9	118.79	59.9	
18	0	0	302.39	152.5	302.39	152.5	
19	0	0	302.39	152.5	302.39	152.5	
20	0	0	302.39	152.5	302.39	152.5	
21	0	0	302.39	152.5	302.39	152.5	
22	0	0	302.39	152.5	302.39	152.5	
23	0	0	302.39	152.4	302.39	152.4	
24	0	0	302.39	152.4	302.39	152.4	
25	0	0	302.39	152.4	302.39	152.4	
26	0	0	302.39	152.4	302.39	152.4	
27	0	0	302.39	152 .4	302.39	152.4	
28	0	0	204.98	103.4	204.98	103.4	
29	-	-	-	-	-	-	
30	-	-	•	-	-	-	
31	-	-	-	-	-	-	
Total	5.85	3.0	7,331.04	3,696.1	7,336.89	3,699.1	

March, 1974

	Maich, 1777					rom
	2/11.24		0.011.3.6.	90'' Meter		
_	36'' Me				36" & 90" N	cfs
Day	A.F.	cfs	A.F.	cfs	A.F	CIS
_	•	^	0	0	0	0
1	0	0	0	0	0	0
2	0	0	0	0	0	0
3	0	0	0	0	0	0
4	0	0	0	0	0,28	0.1
5	0.28	0.1	0	0	0.28	0.1
6	0	0	0	0	0	0
7	0	0	0	0	0	0
8	0	0	0	0	0	0
9	0	0	0		0	0
10	0	0	0	0		0
11	0	0	0	0	0	
12	0	0	0	0	0	0
13	0	0	0	0	0	0
14	0	0	0	0	0	0
15	0	0	0	0	0	0
16	0	0	0	0	0	0
17	0	0	0	0	0	0
18	0	0	0	0	0	0
19	0	0	0	0	0	0
20	0	0	.0	0	0	0
21	6.98	3.5	120.67	60.8	127.65	64.3
22	0	0	200.40	101.0	200.40	101.0
23	0	0	50.83	25.6	50.83	25.6
24	0	0	0	0	0	0
25	5.99	3.1	118.24	59.6	124.23	62.7
26	0	0	196.85	99.3	196.85	99.3
27	0	0	196.85	99.3	196.85	99.3
28	0	0	196.85	99.3	196.85	99.3
29	0	0	196.85	99.2	196.85	99.2
30	0	0	196.85	99.3	196.85	99.3
31	0	0	41.91	21.1	41.91	21.1
Total	13.25	6.7	1,516.30	764.5	1,529.55	771.2

April, 1974

	11, 1, 1, 1			Total 1	From	
	3611 M	leter	90'' M	leter	36" & 90"	Meters
Day	A.F.	cfs	A.F.	cfs	A.F.	cfs
			÷			
1	4.71	2.3	117.70	59.3	122.41	61.6
2	0	0	202.63	102.2	202.63	102.2
3	0	0	199.97	100.8	199.97	100.8
4	0	0	199.26	100.5	199.26	100.5
5	44.69	22.5	107.12	54.0	151.81	76.5
6	101.15	51.0	0	0	101.15	51.0
7	101.15	51.0	0	0	101.15	51.0
8	101.15	51.0	0	0	101.15	51.0
9	101.15	51.0	0	0	101.15	51.0
10	101.15	51.0	0	0	101.15	51.0
11	101.15	51.0	0	0	101.15	51.0
12	101.15	51.0	0	0	101.15	51.0
13	101.15	51.0	0	0	101.15	51.0
14	101.15	51.0	0	0	101.15	51.0
15	101.15	51.0	0	0	101.15	51.0
16	101.15	51.0	0	0	101.15	51.0
17	101.14	51.0	0	0	101.14	51.0
18	101.14	51.0	0	0	101.14	51.0
19	101.14	51.0	0	0	101.14	51.0
20	101.14	51.0	. 0	0	101.14	51.0
21	101.14	51.0	0	0	101.14	51.0
22	101.14	51.0	0	0	101.14	51.0
23	101.14	51.0	0	0	101.14	51.0
24	101.14	51.0	0	0	101.14	51.0
25	101.14	51.0	0	0	101.14	51.0
26	101.14	51.0	0	0	101.14	51.0
27	101.14	51.0	0	0	101.14	51.0
28	25.96	13.1	0	0	25.96	13.1
29	0	0	0	0	0	0
30	0	0	0	0	0	0
31	-	-	-	-	-	-
Total	2,300.55	1,159.9	826.68	416.8	3, 127. 23	1,576.7

May, 1974

					Total From	
	36" N		90'' N	leter	36'' & 90''	Meters
Day	<u>A.F.</u>	cfs	A.F.	cfs	A.F.	cfs
1	0	0	^	_	_	
1 2	0 0	0	0	0	0	0
		0	0	0	0	0
3	22.42	11.3	0	0	22.42	11.3
4	103.35	52.1	0	0	103.35	52.1
5	101.67	51.3	0	0	101.67	51.3
6	37.13	18.7	128.77	64.9	165.90	83.6
7	0	0	200.03	100.9	200.03	100.9
8	0	0	197.86	99.8	19 7. 86	99.8
9	0	0	197.74	99.7	197.74	99.7
10	0	0	193.34	97.5	193.34	9 7. 5
11	0	0	191.64	96.6	191.64	96.6
12	0	0	43.96	22.2	43.96	22.2
13	2.07	1.0	130.18	65.6	132.25	66.6
14	0	0	201.14	101.4	201.14	101.4
15	0	0	200.28	101.0	200.28	101.0
16	0	0	199.33	100.5	199.33	100.5
17	0	0	198.25	100.0	198.25	100.0
18	0	0	200.53	101.1	200.53	101.1
19	0	0	42.01	21.2	42.01	21.2
20	5.19	2.6	125.97	63.5	131.16	66.1
21	0	0	204.98	103.3	204.98	103.3
22	0	0	203.17	102.4	203.17	102.4
23	0	0	202.85	102.3	202.85	102.3
24	0	0	202.53	102.1	202.53	102.1
25	0	0	201.62	101.7	201.62	101.7
26	0	0	269.03	135.6	269.03	135.6
27	0	0	291.67	147.0	291.67	147.0
28	0	0	302.89	152.7	302.89	152.7
29	0	0	303.13	152.8	303.13	152.8
30	0	0	299.90	151.2	299.90	151.2
31	0	0	299.92	151.2	299.92	151.2
Total	271.83	137.0	5,232.72	2,638.2	5,504.55	2,775.2

TABLE NO. C-2

Page 7 of 10

NONTRIBUTARY WATER FROM DEVIL CANYON POWERPLANT AFTERBAY (OC-59T) AS DISCHARGED TO M.W.D. RIALTO PIPELINE FROM 36" AND 90" VENTURI METERS

June, 1974

					Total From		
	36'' M		90'' N	leter	36" & 90"	Meters	
Day	A.F.	cfs	A.F.	cfs	A.F.	cfs	
1	0	0	296.02	149.2	296.02	140.3	
2	0	0	86.96	43.8	86.96	149.2	
3	2.46	1.3	188.95	95.3	191.41	43.8	
4	0	0	302.63	152.6	302.63	96.6	
5	0	0	302.63	152.6		152.6	
6	0	0	302.63	152.6	302.63	152.6	
7	0	0	302.63		302.63	152.6	
8	0	0	302.63	152.6	302.63	152.6	
9	0	0		152.6	302.63	152.6	
10	0	0	302.63	152.6	302.63	152.6	
11	0		302.64	152.5	302.64	152.5	
12	0	0	302.64	152.5	302.64	152.5	
13	0	0	80.76	40.7	80 . 76	40.7	
		0	0	0	0	0	
14	5 . 78	2.9	176.16	88.8	181.94	91.7	
15	0	0	303.47	153.0	303.47	153.0	
16	0	0	87.41	44.1	87.41	44.1	
17	3.42	1.7	183.36	92.4	186.78	9 4 . 1	
18	0	0	301.61	152.1	301.61	152.1	
19	0	0	301.61	152.1	301.61	152.1	
20	0	0	301.61	152.1	301.61	152.1	
21	0	0	301.61	152.1	301.61	152.1	
22	0	0	301.61	152.1	301.61	152.1	
23	0	0	301.61	152.1	301.61	152.1	
24	0	0	301.62	152.1	301.62	152. l	
25	0	0	301.62	152.1	301.62	152. 1	
26	0	0	301.62	152.1	301.62	152.1	
27	0	0	301.62	152.0	301.62	152.0	
28	0	0	301.62	152.0	301.62	152.0	
29	0	0	301.62	152.0	301.62	152.0	
30	0	0	305.63	154.1	305.63	154.1	
31	-	-	-	-	-	-	
Total	11.66	5.9	7,749.16	3,906.9	7,760,82	3,912.8	

July, 1974

	- 4			Total From		
_	36" Meter 90" Mete		leter	36" & 90" Meters		
Day	A.F.	cfs	<u>A.F.</u>	cfs	A.F.	cfs
1	0	0	307 53			
2	0	0	297. 52	150.0	297.52	150.0
3		0	297.52	150.0	297.52	150.0
	0	0	297.52	150.0	297.52	150.0
4	0	0	297.52	150.0	297.52	150.0
5	0	0	297.52	150.0	297.52	150.0
6	0	0	297.52	150.0	297.52	150.0
7	0	0	354.38	178.6	354.38	178.6
8	0	0	396.70	200.0	396.70	200.0
9	0	0	396.70	200.0	396.70	200.0
10	0	0	396.70	200.0	396.70	200.0
11	0	0	396.70	200.0	396.70	200.0
12	0	0	396.70	200.0	396.70	200.0
13	0	0	396.70	200.0	396 . 7 0	200.0
14	4.75	2.4	177.69	89.6	182.44	92.0
15	0	0	396.69	200.0	396.69	200.0
16	0	0	396.69	200.0	396.69	200.0
17	0	0	396. 69	200.0	396.69	200.0
18	0	0	396.69	200.0	396.69	200.0
19	0	0	396.69	200.0	396.69	200.0
20	0	0	396.69	200.0	396.69	200.0
21	0	0	396.69	200.0	396.69	200.0
22	0	0	396.69	200.0	396.69	200.0
23	0	0	396.69	200.0	396.69	200.0
24	0	0	396.69	200.0	396.69	200.0
25	0	0	403.62	203.5	403.62	203.5
26	0	0	407.80	205.6	407.80	205.6
27	0	0	401.65	202.5	401.65	202.5
28	0	0	396.69	200.0	396.69	200.0
29	0	0	396.69	200.0	396.69	200.0
30	0	0	396.70	200.0	396.70	
31	0	0	396.70	200.0	396.70	200.0 200.0
Total	4.75	2.4	11,464.14	5,779.8	11,468.89	5,782.2

NONTRIBUTARY WATER FROM DEVIL CANYON POWERPLANT AFTERBAY (OC-59T) AS DISCHARGED TO M.W.D. RIALTO PIPELINE FROM 36" AND 90" VENTURI METERS

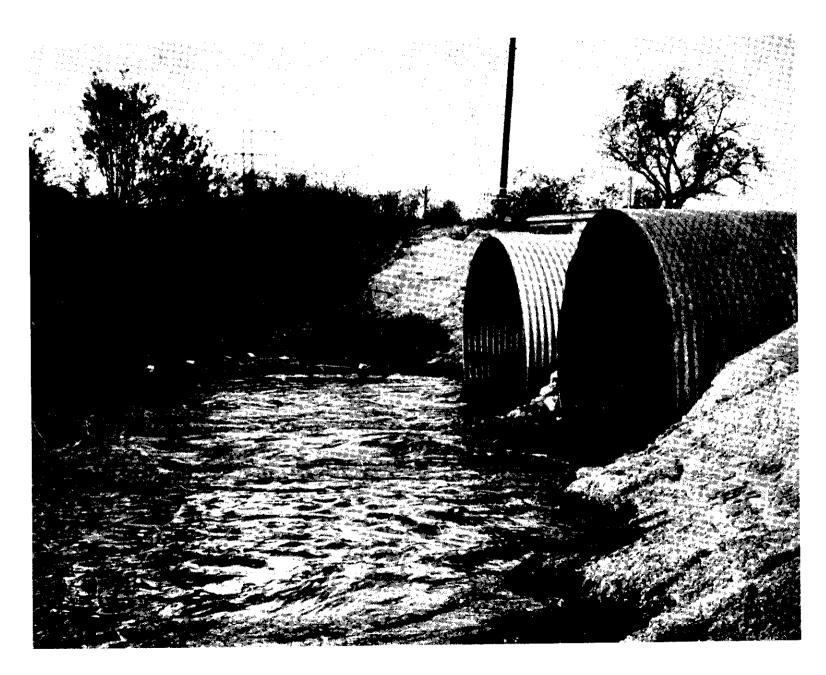
August, 1974

36" Meter			90'' N	Meter	Total From 36'' & 90'' Meters		
Day	A.F.	cfs	A.F.	cfs	A.F.	cfs	
_							
1	0	0	396.69	200.0	396.69	200.0	
2	0	0	396.69	200.0	396.69	200.0	
3	0	0	396.69	200.0	396.69	200.0	
4	0	0	396.69	200.0	396.69	200.0	
5	0	0	396.69	200.0	396.69	200.0	
6	0	0	396.69	200.0	396.69	200.0	
7	0	0	396.69	200.0	396.69	200.0	
8	0	0	396.69	200.0	396.69	200.0	
9	0	0	396.69	200.0	396.69	200.0	
10	0	0	396.69	200.0	396.69	200.0	
11	0	0	396.70	200.0	396.70	200.0	
12	0	0	396.70	200.0	396.70	200.0	
13	0	0	396.70	200.0	396.70	200.0	
14	0	0	396.70	200.0	396.70	200.0	
15	0	0	396.70	200.0	396.70	200.0	
16	0	0	403.97	203.7	403.97	203.7	
17	0	0	400.74	202.0	400.74	202.0	
18	4.78	2.4	173.36	87.4	178.14	89.8	
19	0	0	408.80	206.1	408.80	206.1	
20	0	0	402.05	202.7	402.05	202.7	
21	2.20	1.1	336.78	169.8	338.98	170.9	
22	0	0	404.50	203.9	404.50	203.9	
23	0	0	404.50	203.9	404.50	203.9	
24	0	0	404.50	203.9	404.50	203.9	
25	0	0	404.50	203.9	404.50	203.9	
26	0	0	404.50	203.9	404.50	203.9	
27	0	0	404.50	203.9	404.50		
28	0	0	404.50	203.9	404.50	203.9	
29	0	0	404.50	204.0	404.50	203.9	
30	0	0	404.50	204.0	404.50	204.0	
31	0	0	404.50	204.0	404.50	204.0 204.0	
Total	6.98	3.5	12,121.10	6,111.0	12, 128. 08	6,114.5	

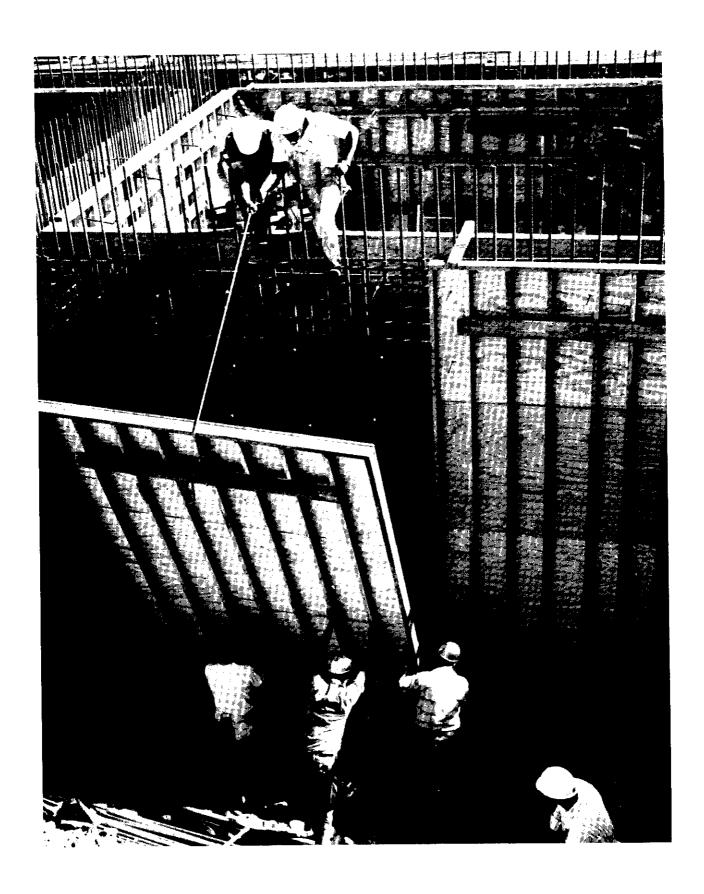
NONTRIBUTARY WATER FROM DEVIL CANYON POWERPLANT AFTERBAY (OC-59T) AS DISCHARGED TO M.W.D. RIALTO PIPELINE FROM 36" AND 90" VENTURI METERS

September, 1974

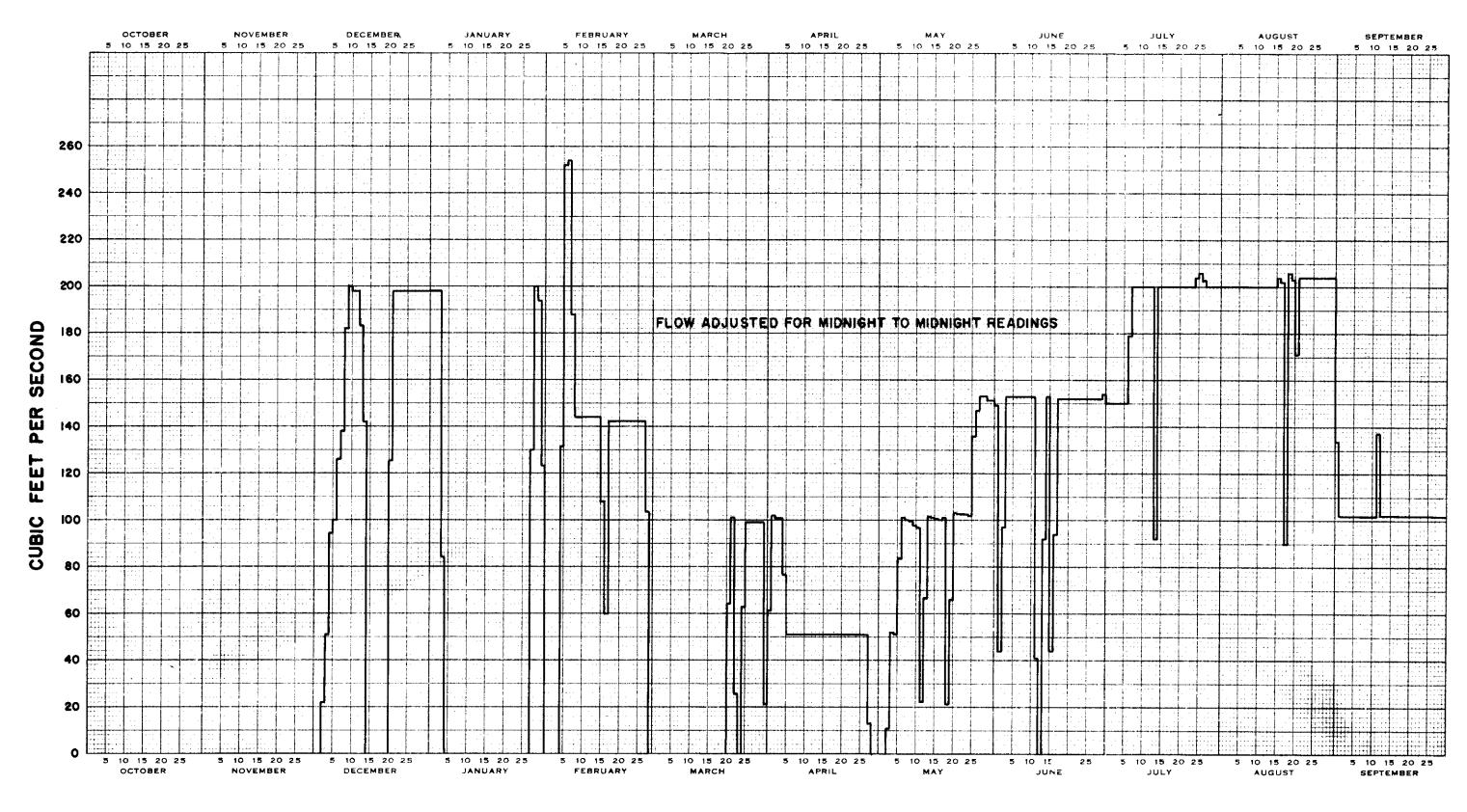
	36'' IV	leter	90'' N	90" Meter		Total From 36" & 90" Meters	
Day	A.F.	cfs	A.F.	cfs	A.F.	cfs	
	•						
1	0	0	265.01	133.6	265.01	133.6	
2	0	0	202.64	102.1	202.64	102.1	
3	0	0	202.64	102.1	202.64	102.1	
4	0	0	202.64	102.1	202.64	102.1	
5	0	0	202.64	102.2	202.64	102.2	
6	0	0	202.64	102.2	202.64	102.2	
7	0	0	202.65	102.2	202.65	102.2	
8	0	0	202.65	102.2	202.65	102.2	
9	0	0	202.65	102.2	202.65	102.2	
10	0	0	202.65	102.2	202.65	102.2	
11	0	0	202.65	102.2	202.65	102.2	
12	0	0	271.36	136.8	271.36	136.8	
13	0	0	201.89	101.8	201.89	101.8	
14	0	0	201.89	101.8	201.89	101.8	
15	0	0	201.89	101.8	201.89	101.8	
16	0	0	201.89	101.8	201.89	101.8	
17	0	0	201.89	101.8	201.89	101.8	
18	0	0	201.89	101.8	201.89	101.8	
19	0	0	201.89	101.8	201.89	101.8	
20	0	0	201.89	101.8	201.89	101.8	
21	0	0	201.89	101.8	201.89	101.8	
22	0	0	201.89	101.8	201.89	101.8	
23	0	0	201.89	101.8	201.89	101.8	
24	0	0	201.89	101.8	201.89	101.8	
25	0	0	201.89	101.8	201.89	101.8	
26	0	0	201.89	101.8	201.89	101.8	
27	0	0	201.89	101.8	201.89	101.8	
28	0	0	201.88	101.7	201.88	101.7	
29	0	0	201.88	101.7	201.88	101.7	
30	0	0	201.88	101.7	201.88	101.7	
31	-	-	-	-	-	-	
Total	0	0 .	6,196.81	3, 124. 2	6 ,1 96.81	3, 124. 2	



Nontributary State Project water flowing in Chino Creek on entrance to Prado Flood Control Basin



Construction of Permanent Connection (OC 59) for State Project Water Delivery into San Antonio Creek located in Montclair - Taken in November 1974



NON-TRIBUTARY WATER RELEASED AT OC-59T FROM DEVIL CANYON POWERPLANT AFTERBAY TO M.W.D. RIALTO PIPELINE
PLATE C-1

APPENDIX D

WATER QUALITY OF SURFACE WATER FLOW OF SANTA ANA RIVER AT PRADO DAM

Prepared By

John M. Toups

1973-74

TABLE NO. D-1

U.S.G.S. WATER QUALITY SAMPLES
BELOW PRADO DAM
WATER YEAR 1973-74

Date	E.C.	T.D.S.	Date	E.C.	T.D.S.
Oct. 1973	1240	761	April 1974	585	356
000. 1773	1300	806	White Told	941	556
	1210	742		945	566
	1220	748		931	56 4
	1220	740		1180	724
Nov. 1973	1250	757		1100	124
11011 1373	1190	730	May 1974	787	463
	1260	785	ray 1974	767	451
	1250	764		740	430
	1250	704		740	430
Dec. 1973	1210	745	June 1974	653	386
2001 2770	714	426		663	376
	1170	706			0.0
	685	400	July 1974	623	362
			-	569	336
Jan. 1974	767	464		583	346
	1050	629		559	325
	1230	735			00
			Aug. 1974	554	329
Feb. 1974	662	483		558	337
1001 17.1	776	444		55 <i>6</i>	325
	773	452		569	326
		.02		551	306
Mar. 1974	1150	674		301	300
	1225	723	Sept. 1974	612	353
	680	393			
	1205	752			
	807	491			

TABLE D-2

WEIGHTED T.D.S. CALCULATION SHEET

BELOW PRADO DAM

WATER YEAR 1973-1974 TDS= 0.62852160(FC)+ -23.846450

MON T H		•DΑΥ	U.S.G.S. MEAN DAILY FLOW	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (E.C.)	MEAN DAILY ADJUSTED T.D.S.	MEAN DAILY FLO TIMES ADJUSTED T.D.
			(CFS-DAY)	(MICROMHOS)	(PPM)	
	ост	1	80.0	1240	756	60480.
	OCT	2	128.0	1240	756	96768.
	OCT	3	163.0	1245	759	123717.
	OCT	4	184.0	1250	762	140208.
	OCT	5	179.0	1260	768	137472.
	OCT	6	155.0	1270	774	119970.
	CCT	7	68.0	1280	781	53108.
	OCT	8	54.0	1290	787	42498.
	OCT	9	49.0	1295	790	38710.
	OCT	10	50.0	1300	7 93	39650.
	OCT	14	45.0	1255	7 65	34425.
_	001	11	54.0	1290	787	42498.
D-N	OCT	12	53.0	1280	781	41393.
10	001	13	48.0	1270	774	37152.
	OCT		54.0	1240	756	40824.
	OCT	_ 16	52.0	1230	74 <i>9</i>	38948.
	OCT	17	52.0	1220	743	386 36 .
	OCT	18	53.0	1210	7 37	39061.
	OCT	19	50.0	1210	737	36850.
	OCT	20	56.0	1210	7 37	41272.
	OCT	21	57.0	1215	740	42180.
	OCT	22	64.0	1215	740	47360.
	OCT	23	66.0	1220	743	49038.
	OCT	24	67.0	1220	743	49781.
	OCT	_ 25	65.0	1220	743	48295.
	OCT	26	63.0	1225	746	46998.
	OCT	27	61.0	1225	746	45506.
	OCT	28	59.0	1230	7 49	44191.
	OCT	29	59.0	1230	749	44191.
	OCT	30	54.0	1235	7 52	40608.
	ост	31	51.0	1235	7 52	38352.

TOTAL.

2293.

1740140.

TABLE D-2

WEIGHTED T.D.S. CALCULATION SHEET

BELOW PRADO DAM

WATER YEAR 1973-1974 TDS= 0.62852160(EC)+ -23.846450

MONTH-		DAY	U.S.G.S. MEAN DAILY FLOW	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (E.C.)	MEAN DAILY ADJUSTED T.D.S.	MEAN DAILY FL(TIMES ADJUSTED T.D.!
			(CFS-DAY)	(MICROMHOS)	(PPM)	
	1101	•	53.0	1240	756	40068.
	NOV	1	58.0	1240	7 56	43848.
	NOV	2 3	55.G	1245	7 59	41745.
	NOV	5 4	57.0	1245	7 59	43263.
	MOV		61.0	1250	762	46482•
	NOV	5	60.0	1250	762	45720•
	NOV	6 7	59.0	1250	762	44958.
	NOV	A A	64.0	1250	762	48768.
	1107	9	63.0	1250	762	48006.
	NOV		61.0	1250	762	46482.
	NOV	10	65.0	1250	762	49530.
Θ	V0 <i>N</i> V0 <i>I</i> 9	11 12	65 . 0	1250	762	49530.
 	MOA	13	64.0	1250	762	48768.
	MOA MOA	14	56.0	1250	762	42672.
	NOA	15	74.0	1250	762	56388.
•	NOV	16	68.0	1260	768	52224.
	NOV	17	78.0	1390	850	66300.
		18	114.0	1411	863	98382.
	NON NON	16 19	110.0	1420	869	95590.
			73.0	1280	781	57013.
	NOV	20	114.6	1222	744	84816.
	NOV	21	169.0	1260	768	129792.
	NOV	22 23	165.0	1200	730	120450.
	V011	23 24	168.0	1120	680	114240.
	VOV		150.0	1290	787	118050.
	NOV	25 56	88.0	1291	788	69344。
	1107	26	76.0	1230	749	56924.
	1101	2 7	77.0	1250	762	58674.
	NOV	28	105.0	1263	770	80850.
	NOV	29	86.0	1290	787	67682.
	иол	30	Ģ 0 • 0	***		
	T.O	AT A I	2556.			1966559.

2556.

TOTAL MONTHLY WEIGHTED T.D.S.

769

TABLE D-2

WEIGHTED T.D.S. CALCULATION SHEET

BELOW PRADO DAM

WATER YEAR 1973-1974 TDS= 0.62852160(EC)+ -23.846450

DEC DEC DEC DEC	1 2	(CFS-DAY) 83.0	CONDUCTANCE (L.C.) (MICROMHOS)	(PPM)	ADJUSTED T.D.!
DEC DEC DEC		ያ ጄ . በ			
DEC DEC DEC		€ 3 • €	1270	774	64242.
DEC Dec	* **	96.0	1210	737	70752.
DEC	٦,	84.0	1230	749	62916.
	4	84.C	1220	743	624 12.
DEC	5	126.0	975	589	74214.
DEC	6	146.0	86 9	522	76212.
DEC	7	206.0	853	512	105472.
DEC	8	215.0	843	506	108790.
				483	93702.
				443	106763.
				423	109134.
				426	108284.
				431	109043.
				429	109395.
				712	111072.
					69657•
					64008.
					62916.
					60434.
					59808.
					64080.
					164724.
					155397.
					127555.
					109060.
					105931.
					106080.
					109483.
					110416.
					109671.
DEC	31	262.0	709	422	110564.
	DEC DEC DEC DEC DEC DEC DEC DEC DEC DEC	DEC 9 DEC 10 DEC 11 DEC 12 DEC 13 DEC 14 DEC 15 DEC 16 DEC 16 DEC 17 DEC 18 DEC 19 DEC 20 DEC 21 DEC 21 DEC 23 DEC 24 DEC 25 DEC 25 DEC 26 DEC 27 DEC 28 DEC 29 DEC 29 DEC 30	DEC 9 194.0 241.0 DEC 10 241.0 DEC 11 258.0 DEC 12 253.0 DEC 13 253.0 DEC 14 255.0 DEC 15 DEC 16 93.0 DEC 17 84.0 DEC 17 84.0 DEC 18 84.0 DEC 19 82.0 DEC 20 84.0 DEC 21 90.0 DEC 21 90.0 DEC 21 90.0 DEC 259.0 DEC 23 277.0 DEC 24 263.0 DEC 24 263.0 DEC 25 266.0 DEC 26 259.0 DEC 27 DEC 28 269.0 DEC 28 DEC 29 DEC 30 268.0 DEC 29 DEC 30 268.0	DEC 9 194.0 743 DEC 10 241.0 743 DEC 11 258.0 711 DEC 12 253.0 719 DEC 13 253.0 724 DEC 14 255.0 721 DEC 15 156.0 1170 DEC 16 93.0 1230 DEC 17 84.0 1250 DEC 18 84.0 1230 DEC 19 82.0 1210 DEC 20 84.0 1170 DEC 21 90.0 1170 DEC 21 90.0 1170 DEC 23 277.0 930 DEC 24 263.0 810 DEC 25 266.0 690 DEC 26 259.0 688 DEC 27 260.0 687 DEC 28 269.0 685 DEC 29 268.0 693 DEC 29 268.0 693 DEC 30 701	DEC 9 194.0 807 483 DEC 10 241.0 743 443 DEC 11 258.0 711 423 DEC 12 253.0 719 426 DEC 13 253.0 724 431 DEC 14 255.0 721 429 DEC 15 156.0 1170 712 DEC 16 93.0 1230 749 DEC 17 84.0 1250 762 DEC 18 84.0 1230 749 DEC 19 82.0 1210 737 DEC 20 84.0 1170 712 DEC 21 90.0 1170 712 DEC 21 90.0 1170 712 DEC 22 259.0 1050 636 DEC 23 277.0 930 561 DEC 24 263.0 810 485 DEC 25 266.0 690 410 DEC 26 27 260.0 687 408 DEC 28 269.0 685 407 DEC 29 268.0 693 412 DEC 29 268.0 693 412

TOTAL

5813.

TABLE D-2

WEIGHTED T.D.S. CALCULATION SHEET

BELOW PRADO DAM

WATER YEAR 1973-1974 TDS= 0.62852160(EC)+ -23.846450

	MONTH-	DAY	U.S.G.S. MEAN Daily Flow	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (F.C.)	MEAN DAILY ANJUSTED T.D.S.	MEAN DAILY FLO TIMES ADJUSTED T.D.!
			(CFS-DAY)	(MICROMHOS)	(PPM)	
	MAL	1	297.0	713	424	125928.
	AAL	1 2	281.0	717	427	119987.
	JAT:	3	275.0	692	411	113025.
	IAU	4 .	395.0	699	415	163925.
	JAN	5	755.C	767	458	345790•
	MAL	6	730.0	689	409	298570.
	MAL	7	760.0	610	360	273600.
	JAN	8	1440.0	516	300	432000.
	JAG	9	794.0	472	273	216762.
	MAL	10	353.0	467	270	95310.
	MAL	11	352.0	499	290	102080.
	JAI	12	346.0	569	334	115564.
	JAN	13	341.0	697	414	141174.
н	\IAU	14	340.0	829	497	168980.
Ψ.5	JAI	15	335.0	958	578	193630.
. •	MAL	16	333.0	1040	630	209790.
	JAH	17	328.0	1090	661	216808.
	JAN	18	308.0	1140	693	213444.
	IAU	19	288.0	1180	718	206784.
	MAL	20	261.0	1160	705	184005.
	IAU	21	227.0	1140	693	157311.
	MAL	22	150.0	1200	73 0	109500.
	JAN	23	104.0	1240	756	78624.
	JAN	24	103.0	1230	749	77147.
	ITAL	25	102.0	1210	737	75174.
	HAU	26	98°C	1200	730	71540.
	MAL	27	94.0	1180	718	67492.
	JAI	28	102.0	756	451	46002.
	JAL	29	233.0	749	447	104151.
	JAM	30	245.0	732	436	106820.
	JAL		263.0	719	428	112564.
	 .					4943481

11033. TOTAL

4943481.

MONTHLY WEIGHTED T.D.S.

TABLE D-2

WEIGHTED T.D.S. CALCULATION SHEET

BELOW PRADO DAM

WATER YEAR 1973-1974 TDS= 0.62852160(EC)+ -23.846450

	MONTH-	-DaY	U.S.G.S. MEAN DAILY FLOW	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (E.C.)	MEAN DAILY ADJUSTED T.D.S.	MEAN DAILY FL TIMES ADJUSTED T.D.
			(CFS-DAY)	(MICROMHOS)	(PPM)	
	FEP	1	232.0	707	421	97672.
	FE6	2	122.0	868	522	63684.
	FEB	3	108.0	1029	623	67284.
	FEB	4	106.0	1190	724	76744.
	FEB	5	117.0	1170	712	83304.
	FEB	6	272.0	685	407	110704.
	FEB	7	308.0	679	403	124124.
	FEB	8	292.0	705	419	122348.
	FED	9	245.0	7 69	459	112455.
	FEB	10	244.0	7 58	453	110532.
	FEB	11	244.0	7 55	451	110044.
	FEB	12	245.0	7 63	456	111720.
	FEB	13	244.0	775	463	112972.
7	FEB	14	248.0	773	462	114576.
φ	FED	15	248.0	7 75	463	114824.
	FEE	16	220.0	808	484	106480.
	FER	17	204.0	857	515	105060.
	FEB	18	196.0	835	501	98196.
	FEF	19	245.0	7 58	453	110985.
	FEB	20	243.0	757	452	109836.
	FEB	21	238.0	7 59	453	107814.
	FEB	22	241.0	767	458	110378.
	FEB	23	243.0	77 5	463	112509.
	FEB	24	237.0	774	463	109731.
	FE6	25	234.0	764	456	106704.
	FER	26	237.0	767	458	108546.
	FEB	27	234.0	768	459	107406.
	FEB	28	239.0	788	471	112569.
	70	TAL	6286.			2939201.
MONTHL	Y WEIGHTED	T.D.S.			468	

TABLE D-2

WEIGHTED T.D.S. CALCULATION SHEET

BELOW PRADO DAM

WATER YEAR 1973-1974 TDS= 0.62852160(EC)+ -23.846450

564

3154890.

	⊴ONTH-I	DAY	U.S.G.S. MEAN DATLY FLOW	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (L.C.)	MEAN DAILY ADJUSTED T.D.S.	MEAN DAILY FLO TIMES ADJUSTED T.D.S
			(CFS-DAY)	(MICROMHOS)	(PPM)	
	MAP	1	174.0	1068	647	112578.
	MAR	2	203.0	905	545	110635.
	HAP	3	231.0	853	512	118272.
	MAR	4	227.0	949	573	130071.
	MAR	5	181.0	1140	693	125433.
	MAR	6	148.0	1230	749	110852.
	MAR	7	141.0	1200	730	102930.
	MAR	8်	162.0	734	437	70794.
	MAR	9	180.0	603	355	63900.
	MAR	10	180.0	557	326	58680.
	MAR	11	194.0	636	376	72944.
	MAR	12	206.0	711	423	87138.
	MAR	13	204.0	842	505	103020.
Ħ	MAR	14	202.0	97 5	589	118978.
₽7	MAR	15	197.0	1050	636	125292.
	MAR	16	195.0	1090	661	128895.
	MAR	17	191.0	1150	699	133509.
	MAR	18	187.0	1190	724	135388.
	MAR	19	180.0	1170	712	128160.
	MAR	20	166.0	1215	740	122840.
	MAR	21	123.0	1220	743	91389.
	MAR	22	153.0	856	514	78642.
	MAR	23	162.0	839	503	81486.
	MAR	24	150.0	1080	655	98250.
	MAR	25	1.10.0	1140	693	76230.
	MAR	26	146.0	813	487	71102.
	MAR	27	156.0	803	481	75036.
	MAR	28	209.0	791	473	98857.
	MAR	29	231.0	840	504	116424.
	MAR	30	210.0	848	509	106890.
	MAR	31	191.0	873	525	100275.

5590.

TOTAL

MONTHLY WEIGHTED T.D.S.

TABLE D-2 WEIGHTED T.D.S. CALCULATION SHEET

BELOW PRADO DAM

WATER YEAR 1973-1974 TDS= 0.62852160(EC)+ -23.846450

545

2158141.

	MONTH-	EAY	U.S.G.S. MEAN DAILY FLOW	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (E.C.)	MEAN DAILY ADJUSTED T.D.S.	MEAN DAILY FLO TIMES ADJUSTED T.D.
			(CFS-DAY)	(MICROMHOS)	· (PPM)	
	AFR	1	110.0	1077	653	71830.
	ΛPP	Ž	235.0	678	402	94470.
	APR	3	258.0	7 80	466	120228.
	APR	4	213.0	846	508	108204.
	APR	5	193.0	838	503	970 7 9.
	APR	6	140.0	941	568	79520.
	ΛPR	7	128.0	934	563	72064.
	ΔPR	8	119.0	925	558	66402.
	APR	9	119.0	953	5 7 5	68425.
	APR	10	123.0	954	57 6	70848.
	APR	11	122.0	940	567	69174.
	APR	12	120.0	928	559	67080.
	APR	13	120.0	922	556	66720.
	APR	14	117.0	910	548	64116.
₽	ΛPP	15	114.0	903	544	62016.
œ	ΛPR	16	116.0	913	550	63800.
	ΛPR	17	109.0	912	549	59841.
	APR	18	112.0	922	556	62272.
	APF	19	119.0	940	567	67473.
	APR	20	128.0	930	561	71808.
	APR	21	124.0	921	555	68820.
	APR	22	127.0	915	551	69977。
	APR	23	126.0	91 0	548	69048.
	APR	24	126.0	9 25	558	70308.
	APR	25	124.0	923	556	68944.
	APP	26	129.0	918	553	71337.
	APR	27	126.0	9 22	556	70056.
	APR	28	117.0	908	547	63999.
	APR	29	75. 0	1120	680	51000.
	APR	30	74.0	1140	693	51282.
						0450444

3963.

TOTAL.

MONTHLY WEIGHTED T.D.S.

TABLE D-2

WEIGHTED T.D.S. CALCULATION SHEET

BELOW PRADO DAM

WATER YEAR 1973-1974 TDS= 0.62852160(EC)+ -23.846450

	wCMTH-	-ΓΑΥ	U.S.G.S. MEAN Daily flow	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (L.C.)	MEAN DAILY ADJUSTED T.D.S.	MEAN DAILY FLO TIMES ADJUSTED T.D.
			(CFS-DAY)	(MICROMHOS)	(PPM)	
	MA1	1	67. 0	1170	712	47704.
	MAY	2	68.0	1170	712	48416.
	MAY	3	67.0	1160	705	47235.
	MAY	4	95.0	1027	622	59090.
	MAY	5	128.0	891	536	68608.
	MAY	6	155.0	853	512	79360.
	MAY	7	186.0	7 65	45 7	85002.
	MAA	8	187.0	777	465	86955.
	MAY	9	186.0	788	471	87606.
	MAY	10	182.0	779	466	84812.
	MAY	11	174.0	773	462	80388.
	ΜŅŸ	12	150.0	805	482	72300.
	MAY	13	87.0	1049	635	55245.
П	MAY	14	172.0	745	444	76368.
₽9	MΛΥ	15	173.0	741	442	76466.
_	MAY	16	168.0	751	448	75264.
	MAY	17	165.0	740	441	72765.
	MΛΥ	18	162.0	733	437	70794.
	MAY	19	142.0	770	460	65320.
	MAY	20	77. 0	1049	635	48895.
	MAY	21	165.0	731	436	71940.
	MAY	22	172.0	730	435	74820.
	MAY	23	170.0	747	446	75820.
	MAY	24	169.0	749	447	75543.
	MAY	25	160.0	741	442	70720.
	млү	26	159.0	717	427	67893.
	MAY	27	187.0	668	396	74052.
	MAY	28	179.0	646	382	68378.
	MAY	29	179.0	651	385	68915.
	MAY	- 30	175.0	641	379	66325.
	MAY	31	178.0	642	380	67640.

TOTAL MORTHLY WEIGHTED T.D.S. 4684.

463

TABLE D-2

WEIGHTED T.D.S. CALCULATION SHEET

BELOW PRADO DAM

WATER YEAR 1973-1974 TDS= 0.62852160(EC)+ -23.846450

	MONTH-EAY	U.S.G.S. MEAN DAILY FLOW	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (E.C.)	MEAN DAILY ADJUSTED T.D.S.	MEAN DAILY FL TIMES ADJUSTED T.D.
		(CFS-DAY)	(MICROMHOS)	(PPM)	AD003(ED 1404
	JUI₄ 1	183.0	653	387	70821.
	S 7UU	159.0	716	426	67734.
	JUN 3	76.0	1030	624	47424.
	JUN 4	199.0	660	391	77809.
	JUN 5	205.0	656	388	79540.
	JUH 6	206.0	668	396	81576.
	Jun: 7	215.0	688	409	87935.
	ปบเง ล	213.0	682	405	86265.
	9 NUG	212.0	663	393	83316.
	JUH 10	212.0	651	385	81620.
	JUN 11	216.0	654	387	83592.
	JUL 12	186.0	733	437	81282.
	JUN 13	69.0	1100	668	46092.
모	JUN 14	70.0	1063	644	45080.
D-10	JUN 15	201.0	645	382	76782.
_	JUI: 16	172.0	660	391	67252.
	JUN 17	69.0	992	600	41400.
	JUN 18	198.0	662	392	77616.
	JUN 19	197.0	654	387	76239.
	JUN 20	194.0	648	383	74302.
	JUM 21	189.0	648	383	72387.
	JUN 22	189.0	646	38 <i>2</i>	72198.
	JUN 23	189.0	637	377	71253.
	JUN 24	181.0	625	369	66789.
	JUN 25	174.0	618	365	63510.
	JUN 26	173.0	621	366	63318.
	JUN 2 7	166.0	614	362	60092.
	JUN 28	169.0	616	363	61347.
	JUN 29	171.0	612	361	61731.
	JUI: 30	176.0	619	365	64240.

5229.

TOTAL MONTHLY WEIGHTER T.D.S.

400

TABLE D-2

WEIGHTED T.D.S. CALCULATION SHEET

BELOW PRADO DAM

WATER YEAR 1973-1974 TDS= 0.62852160(EC)+ -23.846450

	MONTH-L	DAY	U.S.G.S. MEAN DAILY FLOW	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (E.C.)	MEAN DAILY ADJUSTED T.D.S.	MEAN DAILY FL TIMES ADJUSTED T.D.
			(CFS-DAY)	(MICROMHOS)	(PPM)	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
	JUL	1	179.0	617	364	65156.
	JUL.	2	181.0	608	358	64798.
	JUL	3	184.0	606	357	65688.
	JUL	4	179.0	601	354	63366.
	JUL	5	178.0	595	350	62300.
	JUL	6	176.0	595	350	61600.
	JUL	7	184.0	586	344	63296.
	JUL	В	207.0	565	331	68517.
	JUL	9	209.0	565	331	69179.
	JUL	10	212.0	564	331	70172.
	JUL	11	217.0	568	333	72261.
	JUL	12	216.0	564	331	71496.
	JUL	13	216.0	557	326	70416.
	JUL	14	175.0	612	361	63175.
	JUL	15	176.0	663	393	69168.
P11	JUL.	16	217. Ր	562	329	71393.
11	JUL	17	217.0	548	321	69657.
	JUL.	18	215.0	544	318	68370.
	JUL.	19	219.0	546	319	69861.
	JUL	20	218.0	541	316	68888.
	JUL	21	208.0	540	31 6	65728.
	JUL	22	203.0	543	317	64351.
	JUL	23	209.0	548	321	67089.
	JUL	24	209.0	547	320	66880.
	JUL.	25	213.0	555	325	69225.
	JUL	26	217.0	553	324	70308.
	JUL	27	216.0	534	312	67392.
	JUL	28	215. 0	546	319	68585.
	JUL	29	218.0	54 7	320	69760.
	JUL	30	228.0	558	327	74556.
	JUL	31	230.0	562	329	75670.
	тот	ΓAL.	6341.			2108301.

MORTHLY WEIGHTED T.D.S.

332

TABLE D-2

WEIGHTED T.D.S. CALCULATION SHEET

BELOW PRADO DAM

WATER YEAR 1973-1974 TDS= 0.62852160(EC)+ -23.846450

	MONTH-	DAY	U.S.G.S. MEAN Daily Flow	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (E.C.)	MEAN DAILY ADJUSTED T.D.S.	MEAN DAILY FLO TIMES ADJUSTED T.D.
			(CFS-DAY)	(MICROMHOS)	(PPM)	
	AUG	1	230.0	557	326	74980.
	ΛUG	2	233.0	54 9	321	74793.
	ΛUG	3	232.0	550	322	74704.
	ΛUG	4	232.0	560	328	76096.
	AUG	5	229.0	55 7	326	74654.
	AUG	6	229.0	554	324	74196.
	AUG	7	229.0	550	322	73738.
	aua	8	230.0	550	322	74060.
	AUG	9	232.0	547	320	74240.
	AUG	10	228.0	545	319	72732.
	AUC .	11	224.0	536	313	70112.
	AUG	12	223.Ú	541	316	70468.
	AUG	13	227.0	56 7	333	75591.
	AUG	14	227.0	561	329	74683.
. ヤ	AUG	15	226.0	562	329	74354.
P-12	AUG	16	225.0	56 3	330	74250.
10	AUG	17	224.0	55 9	327	73248.
	AUG	18	175.0	655	388	67900.
	AUG	19	177.0	563	330	58410.
	ΛUG	20	224.0	571	335	75040.
	AUG	21	205.C	604	356	72980.
	AUG	22	215.0	561	329	70735.
	ΛŪĞ	23	221.0	556	326	72046.
	AUG	24	223.0	555	325	72475.
	AUG		220.0	550	322	70840.
	AUG	26	216.0	542	317	68472.
	ΛUG	27	216.0	544	318	68688.
	AUG	28	213.0	540	316	67308.
	AUG	29	213.0	532	311	66243.
	AUG	30	214.0	534	312	66768.
	AUG	31	214.0	531	310	66340.

TOTAL

6826.

TABLE D-2

WEIGHTED T.D.S. CALCULATION SHEET

BELOW PRADO DAM

WATER YEAR 1973-1974 TDS= 0.62852160(EC)+ -23.846450

	MONTH-E	CAY	U.S.G.S. MEAN DAILY FLOW	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (E.C.)	MEAN DAILY ADJUSTED T.D.S.	MEAN DAILY FLOO TIMES ADJUSTED T.D.S
			(CFS-DAY)	(MICROMHOS)	(PPM)	
	ern	•	197.0	547	320	63040.
	SEP	1	130.0	605	356	46280.
	SEP SEP	2 3	130.0	593	349	45370.
	SEP	4	131.0	594	349	45719.
	SEP	5	130.0	593	349	45370.
	SEP	6	128.0	590	347	44416.
	SEP	7	129.0	593	349	45021.
	SEP	Å	132.0	603	355	46860.
	SEP	9	133.0	598	352	46816.
	SEP	10	133.0	606	357	47481.
	SEP	11	137.0	614	362	49594.
	SEF	12	152.0	617	364	55328.
	SEP	13	154.0	611	360	55440.
	SEP	14	136.0	625	369	50184.
D -13	SEP	15	138.0	619	365	50370.
.13	SEP	16	136.0	608	358	48688.
	SEP	17	135.0	612	361	48735.
	SEP	18	136.0	622	367	49912.
	SEP	19	141.0	632	373	52593.
	SEP	20	141.6	626	370	52170.
	SEP	21	139.0	625	369	51291.
	SEP -		135.0	609	359	48465.
	SEP	23	133.0	596	351	46683.
	SEP	24	134.0	596	351	47034.
	SEP	25	134.0	602	3 55	47570.
	SEP	26	136.0	611	360	48960.
		27	140.0	622	367	51380.
	SEP	28	137.0	618	365	50005.
	SEP	29	137.0	626	370	50690.
	SEP	3 0	134.0	622	367	49178.
	3EF	30	134.0	UE E	5 57	
	TOT	TAL	4138.			1480643.

TOTAL MONTHLY WEIGHTED T.D.S.

358

TABLE NO. D-3

SUMMARY OF WEIGHTED TDS BELOW PRADO DAM WATER YEAR 1973-74

	Monthly Flow cfs-day	Monthly Flow Times TDS	Monthly Weighted TDS
October	2,293	1,740,140	759
November	2,556	1,966,559	769
December	5,813	2,962,187	510
January	11,033	4,943,481	448
February	6,286	2,939,201	468
March	5,590	3,154,890	564
April	3,963	2,158,141	545
May	4,684	2,170,639	463
June	5,229	2,090,542	400
July	6,341	2,108,301	332
August	6,826	2,221,144	325
September	4,138	1,480,643	358
Total	64,752	29,935,868	<u> </u>
Yearly Weighted TD	S		462

TABLE NO. D-4

SUMMARY OF WEIGHTED TDS OF NONTRIBUTARY WATER RELEASED FROM OC-59T FOR WATER YEAR 1973-74

	Monthly Flow cfs-day	Monthly Flow Times TDS	Monthly Weighted TDS
October	0	0	0
November	0	0	0
December	3,732	824,707	221
January	1,322	265,390	201
February	3,699	747,337	202
March	771	158,950	206
April	1,577	336,621	213
May	2,775	620,914	224
June	3,913	916,638	234
July	5,782	1,247,799	216
August	6,114	1,357,600	222
September	3,124	667,027	214
Total	32,809	7,142,983	
Yearly Weighted TD	s		218

APPENDIX E

WATER QUALITY OF SURFACE
WATER FLOW OF SANTA ANA
RIVER AT RIVERSIDE NARROWS
and
WATER QUALITY OF THE RIVER-

WATER QUALITY OF THE RIVER-SIDE WATER QUALITY CONTROL PLANT AT RIVERSIDE NARROWS

by

Albert A. Webb

1973-74

U.S.G.S. WATER QUALITY SAMPLES M.W.D. CROSSING WATER YEAR 1973-74

Date	E.C.	T.D.S.
1973 October	1120	687
	1090	681
	1100	681
	1110	675
November	1080	670
	1090	673
· ·	1120	688
	1110	706
December	1090	688
'	1090	676
	1090	658
	1080 1040	666
1974 January	297	636 190
	882	533
	1110	400
February	1100	772
rebluary	1140	702
	1080	659
	1100	668
March	1090	658
Match	1110	660
	1080	673
	1070	669
April	1100	680
	1100	680
	1090	682
	1100	689
	1100	691
May	1080	670 .
	1100	677
	1100	681
	1090	695
June	1090	677
<u>-</u>	1090	682
	1100	680
	1100	676
July	1100	674
-	1100	701
٠	1100	701
	1100	691
August	1090	695.
	1100	. 698
	1100	689
	1090	685
	1100	683
September	1090	673
	1110	703
	1090	704
	1110	· 707

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WEIGHTED T.D.S. CALCULATION SHEET

WATER YEAR 1973-74

T.D.S. = $\frac{EC}{0.000051(EC)+1.549790}$

Adjusted T.D.S. Times Mean Daily Flow U.S.G.S. Storm Base Mean Daily Total Flow Flow U.S.G.S. Mean Storm Base U.S.G.S. Mean Daily Flow Flow Flow Daily Specific Adjusted T.D.S. Flow Month-Day Conductance (E.C.) (PPM) (cfs-Day) (cfs-Day) (cfs-Day) (Micromhos) 13243. 1120 697 13243. ٥. OCT 19.0 0.0 19.0 14133. 1080 673 14133. OCT 2 21.0 0.0 21.0 13460. 1080 OCT 20.0 0.0 20.0 673 13460. ٥. 12901. 12901-OCT 19+0 0.0 19.0 1090 679 0. 14133. 1080 673 14133. ٥. OCT 21.0 0.0 21.0 1060 661 13861. ٥. 13861. OCT 21.0 21.0 0.0 1090 14938. 14938. 0.0 22.0 679 OCT 22.0 1090 14259. 679 14259. OCT 21.0 0.0 21.0 1070 0. 14674. 667 14674. 0.0 22.0 OCT 22.0 1080 673 14133. 0. 14133. OCT 21.0 0.0 21.0 0. 14259. 1090 679 14259+ OCT 0.0 21.0 21.0 OCT 0.0 1110 691 14511. 14511. 21.0 21.0 14511. OCT 13 0.0 21.0 1110 691 14511. ٥. 21.0 14511. OCT 0.0 21.0 1110 691 14511. 0. 21.0 14355. 1100 685 14385. 21.0 0.0 21.0 0. 14511. 1110 691 14511. OCT 16 21.0 0.0 21.0 0. 1100 13015. 13015. OCT 17 19.0 0.0 19.0 685 ٥. 13129. OCT 19.0 19+0 1110 691 13129. ٥. 0.0 13015. 0.0 19.0 1100 685 13015. 0. OCT 19.0 1090 679 13580. 0. 13580. 20 20.0 20.0 0.0 21 1090 679 13560. ٥. 13560. OCT 20.0 20.0 0.0 1090 13580. OCT 22 679 13580. 0. 20.0 20.0 0.0 14007. 23 1070 667 14007. 0. OCT 21.0 21.0 0.0 13651. OCT 21.0 21.0 1060 661 13631. 0.0 138â1. 1060 13661. OCT 25 21.0 0.0 21.0 661 0. 13881. 1060 13681. OCT 26 21.0 21.0 661 0. 0.0 1070 13340. 13340. 667 0. OCT 27 20.0 0.0 20.0 1090 13560. 13580. 679 ٥. OCT 28 70.0 0.0 20.0 1070 667 14674. 14674. OCT 29 22.0 22.0 0. 0.0 1070 12673. 12673. OCT 30 19.0 19.0 667 ٥. 0.0 12559. 19.0 1060 12559. OCT 31 19.0 428818. 428818. 634.

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MONTHLY WEIGHTED T.D.S.

M.W.D. CROSSING

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WEIGHTED T.D.S. CALCULATION SHEET

M.W.D. CROSSING

WATER YEAR 1973-74

 $r.b.s. = \frac{EC}{0.000051(EC) + 1.549790}$

	•		•		<u>. </u>	Adjusted T.D.S. Times Mean Daily Flow			
	Month-Day	U.S.G.S. Mean Daily Flow	Storm Flow	Base Flow	U.S.G.S. Mean Daily Specific Conductance (E.C.)	Mean Daily . Adjusted T.D.S.	U.S.G.S. Total Flow	Storm Flow	Base Flow
		(cfs-Day)	(cfs-Day)	(cfs-Day)	(Micromhos)	(PPM)	<u> </u>		
	NOV 1	20.0	0.0	20.0	1080	673	13460.	0.	13460.
	NOV 2	20.0	0.0	20.0	1070	667	13340.	0.	13340.
	NCV 3	20.0	0.0	20.0	1090	679	13580.	0.	13580.
	NOV 4	21.0	0.0	21.0	1060 .	673	14133.	٥.	14133.
	NOV 5	21.0	0.0	21.0	1070	667	14007.	Q.	14007.
(T)	NOV 6	20.0	0.0	20.0	1060	661	13220•	. 0.	13220.
i"	NOV 7	21.0	0.0	21.0	1060	661	13881.	0.	13881.
w	B VCM	22.0	0.0	22.0	1060	661	14542.	0.	14542.
-	NOV 9	23+0	0.0	23.0	1070	667	15341.	0.	15341.
•	NOV 10	22 • C	0.0	22.0	1060	661	14542.	0.	14542.
**	NOV 11	23.0	0.0	23.0	1070	667	15341.	Q •	15341.
	NOV 12	22.0	0.0	22.0	1060	661	14542+	0.	14542.
	NOV 13	22.0	0.0	22.0	1060 (1)	661 ,	14542.	. O•	14542.
-	NCV 14	23.0	0.0	23.0	1060	661	15203.	0.	15203.
	NOV 15	22.0	0.0	22.0	1060	661	14542.	0•	14542.
	NOV 16	21.0	0.0	21.0	1052 (1)	656	13776.	0•	13776.
	NOV 17	27.0	5 . 8	21.2	- 1045 (1)	652 - 665*	17604.	3506.	14098.
	NOV 18	90.0	68.6	21.4	1038 (1)	648 665*	58320.	44099.	14,231.
	NOV 19	43.0	21.5	21.5	1030	643 665*	27649.	13351.	14298•
	OS VON	32.0	10.3	21.7	1090	679 665#	21728.	7298.	14430.
	NOV 21	32.0	10.1	21.9	1110	691 665*	22112•	7548.	14564.
	NOV 22	33.0	10.9	22.1	1110	691 665#	22803.	8106.	14697.
	NOV 23	79.0	56.7	22.3	835	524 665 *	41396	26566.	14830.
	NOV 24	34.0	11.5	22.5	1030	673 665 *	22882.	7919.	14963.
	NOV 25	32.0	9.4	22.6	1080	673 665 ≠	21536.	6507•	15029.
	NOV 26	* 29.0	6.2	22.8	1090	679 665.≠	19691.	4529.	15162.
	NOV 27	23+0	0.0	23.0	1080	673	15479.	Q• <u>*</u>	15479.
	NOV 2B	» 23·0	0.0	23.0	1070	667	15341.	0 •	15341.
	NOV 29	23.0	0.0	23.0	1050	661	15203.	0.	15203•
	NOV 30	23.0	0.0	23.0	1050	655	15065.	0.	15065.
	TOTAL	866.	211+0	655.0			564801.	179419.	435382.
MONTHLY W	EIGHTED T.D.S.				·	652	•	•	

⁽¹⁾ Daily mean E.C. not recorded by U.S.G.S., E.C. estimated by interpolation. *Adjusted T.D.S., for Base Flow, calculated by averaging the T.D.S. on the day before and the day after Storm Flow.

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WEIGHTED T.D.S. CALCULATION SHEET

M.W.D. CROSSING

WATER YEAR 1973-74

T.D.S. = $\frac{EC}{0.000051(EC) + 1.54979}$

	-						Adjusted T.	D.S. Times Mean	Daily Flow
	Month-Day	U.S.G.S. Mean Daily Flow	Storm Flow	Base Flow	U.S.G.S. Mean Daily Specific Conductance (E.C.)	Mean Daily Adjusted T.D.S.	U.S.G.S. Total Flow	Storm Flow	Base Flow
		(cfs-Day)	(cfs-Day)	(cfs-Day)	(Micromhos)	(PPM)	· · · · · · · · · · · · · · · · · · ·		
	DEC 1	27.0	. 4.0	23.0	1055 (1)	658 658 *	17766.	2632.	15134.
	DEC 2	23.0	0.0	23.0	1060	661	15203.	0.	15203.
	DEC 3	22.0	0.0	22.0	1090	679	14938.	Ŏ.	14938.
	DEC 4	22:0	0.0	22.0	1070	667	14674.	ŏ.	14674.
	DEC 5	22.3	0.0	22.0	1060	661	14542.	ŏ.	14542.
Ħ	DEC 6	22.0	0.0	22.0	1080	673	14806.		14806.
(7)	DEC 7	23.0	0.0	23.0	1080	673	15479.	ŏ.	15479.
4.	DEC 8	22+0	0.0	22.0	1070	667	14674	ŏ.	14674.
	DEC 9	21.0	0.0	21.0	. 1077 (1)	671	14091	ŏ.	14091.
•	DEC 10	22.0	0.0	22.0	1083 (1)	675	14850.	0.	14850.
	DEC 11	23.0	0.0	23.0	1090	679	15617.	ō.	15617.
	DEC 12	22.0	0.0	. 22.0	1088 (1)	678	14916.	ō.	14916.
	DEC 12	22.0	0.0	22.0	1086 (1)	677	14894	0.	14894.
	DEC 14	23.0	0.0	23.0	1083 (1)	675	15525.	0.	15525.
1	DEC 15	23.0	0.0	23.0	1081 (1)	674	15502.	0.	15502.
,	DEC 16	23.0	0.0	23.0	1079 (1)	672	15456 •	0.	15456.
	DEC 17	23.0	0.0	23.0 ~	- 1077 (1)	671	15433.	0.	15433.
	DEC 18	23.0	0.0	23.0	1074 (1)	669	15387.	ŏ.	15387.
	DEC 19	23.0	0.0	23.0	1072 (1)	668	15364.	. 0.	15364.
_	DEC 20	- 24.0	0.0	24.0	1070	667	16008.	ŏ.	16008.
	DEC 21	25.0	0.0	25.0	1090	679	16975.	ŏ.	16975.
	DEC 22	24+0	0.0	24.0	1080	673	16152.	0.	16152.
	DEC 23	24.0	0.0	24.0	1060	661	15864.	. 0.	15864.
	DEC 24	24.0	0.0	24.0	1090	679	16296.	ŏ. ·	16296.
	DEC 25	24.0	0.0	24.0	1110	691	16584.	0.	16584.
	· DEC 26	24.0	0.0	24.0	1070	667	16008.	ŏ.	16008.
	DEC 27	24.0	0.0	24.0	1060	661	15864.	ŏ.	15864.
	DEC 28	28.0	0.0	28.0	1080	673	18844.	ŏ.	18844.
	DEC 29	24.0	0.0	24.0	1080	673	16152.	ŏ.	16152.
	DEC 30	24.0	0.0	24.0	1090	679	16296.	0.	16296.
	DEC 31	23.0	0.0	23.0	1070	667	15341.	ŏ.	15341.
MONTHLY 1	TOTAL WEIGHTED T.D.S.	723.	4.0	719.0		672	485501.	2632.	482869.

⁽¹⁾ Daily mean E.C. not recorded by U.S.G.S., E.G. estimated by interpolation. *Adjusted T.D.S., for Base Flow, calculated by averaging the T.D.S. on the day before and the day after Storm Flow.

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WEIGHTED T.D.S. CALCULATION SHEET

M.W.D. CROSSING

WATER YEAR 1973-74

T.D.S. = $\frac{EC}{0.000051(EC)+1.549790}$

									Adjusted T.1).S. Times Mean	Daily Flow
	Month-Da	У	U.S.G.S. Mean Daily Flow	Storm Flow	Base Flow	U.S.G.S. Mean Daily Specific Conductance (E.C.)		Daily .	U.S.G.S. Total Flow	Storm Flow	Base Flow
			(cfs-Day)	(cfs-Day)	(cfs-Day)	(Micromhos)	(PI	M)			
	JAN	•	39.0	15.9	23.1	1040 (1)	649	667 *	25311•	903.	15408.
		2	28+0	4.7	23.3	1010	631	667 *	17663.	2127.	15541•
		3	25.0	1.6	23.4	1010 (1)	631	667 *	15775.	- 167.	15608.
	JAN	4	663.0	639.4	23.6	402	256	667 *	169726	153957.	15741.
	-	5	476.0	452.3	23.7	452	287	667 *	136612.	120804.	15808.
		6	71.0	47.1	23.9	807	507	667 *	35997.	20056.	15941.
<u>ন</u>	JAN	ž .	999.0	975.0	24.0	392	250	667 *	249750.	233742.	16008.
Un	JAN		900.0	875.9	24+1	508	322	667 *	289800.	273725	16075.
. 01		ğ	68.0	43.7	24.3	776	488	667 *	33184.	16976.	16208.
		.ó	61.0	36.6	24:4	757	477	667 *	29097.		16275.
	JAN 1		64.0	39.4	24.6	716	453	667 *	28992	12022. 12584.	16408.
	JAN 1		51.0	26.3	24.7	837	526	667 *	26826.	10351.	16475.
	JAN 1		48.0	23.1	24.9	958	599	667 *	28752.	12144.	16608
	JAN 1		49.0	24.0	25.0	1010	631	667 *	30919.		16675.
	JAN 1		40.0	14.9	25.1	1070	667	667 *	26650.	14244.	16742.
	JAN 1		38.0	12.7	25.3	1060	661	667 *	25118.	9938.	16875.
	JAN 1		40.0	14.6	25.4 ~-		622 -	667 *	24880.	8243. 7938.	16942.
	JAN 1		35+0	9.4	25.6	1070	667	667 *	23345.	6270.	17075.
		9	31.0	5.3	25.7	1080	673	667 *	20863.		17142.
		Ó	31.0	5.1	25.9	1040	649	667 *	20119.	3721. 2844.	17275.
		1	26+0	0.0	26.0	1070	667	•••	17342.	2044	17342.
		2	24.0	0.0	24.0	1060	661		15864.	0.	
•		3	24.0	0.0	24.0	1050	655		15720	0.	15864.
•		4	24.0	0.0	24.0	1070	667	•	16008	0.	15720.
		5	27.0	0.0	27.0	1090	679		18333.		16008.
		6	30.0	0.0	30.č	1030	673		20190.	0. 0.	18333.
		7	32.0	0.0	32.0	1090	679		21728.	0.	Z0190. 21728.
	JAN 2		34 0	0.0	34.0	1110	691		23494.	0.	
		9	33.0	0.0	33.0	1130	703		23199.	0.	23494.
•		ó	33.0	0.0	33.0	1150	715		23595	0.	23199. 23595.
	JAN 3		31.0	0.0	31.0	1140	709		21979.	0.	23393.
											617174
MONTHLY 1	TOTA • EIGHTED T	_	4075.	3267.0	0.805	•	362		1476868	. 932586.	5442#2.

⁽¹⁾ Daily mean E.C. not recorded by U.S.G.S., E.C. estimated by interpolation. *Adjusted T.D.S., for Base Flow, calculated by averaging the T.D.S. on the day before and the day after Storm Flow.

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WEIGHTED T.D.S. CALCULATION SHEET

M.W.D. CROSSING

WATER YEAR 1973-74

T.D.S. = $\frac{EC}{0.000051(EC)+1.549790}$

	-		· · · · · ·				Adjusted T.D	.S. Times Mean	Daily Flow
	Month-Day	U.S.G.S. Mean Daily Flow	Storm Flow	Base Flow	U.S.G.S. Mean Daily Specific Conductance (E.C.)	Mean Daily Adjusted T.D.S.	U.S.G.S. Total Flow	Storm Flow	Base Flow
		(cfs-Day)	(cfs-Day)	(cfs-Day)	(Micromhos)	(PPM)	·	<u> </u>	
	FEB 1	37•0	0.0	37.0	1140	709	26233•	0.	26233.
	FEB 2	34.0	0.0	34.0	1110	691	23494.	0.	23494.
	FEB 3	31.0	0.0	31.0	1120	697	21607.	0.	21607.
	FE5 4	31.0	0.0	31.0	1100	685	21235.	٥.	21235.
[7]	FE9 5	31.0	0.0	31.0	1080	673	20863.	0.	20863.
اج	FEB 6	30.0	0.0	30.0	1050	655	19650.	. 0.	19650.
5	FEB 7	29.0	0.0	29.0	1070	667 .	19343.	0.	19343.
.	F58 8	31.0	0.0	31.0	. 1070	667	20677.	0.	20677.
	FEB 9	32.0	0.0	32.0	1070	667	21344.	. 0.	21344.
•	FEB 10	32.0	0.0	32.0	1055 (1)	664	21248.	0.	21248.
	FE3 11 ·	32+0	0.0	32.0	1060	661	21152.	٥.	21152.
	FEB 12	33.0	0.0	33.0	1070	667	22011.	0.	22011.
	FEB 13	33.0	0.0	33.0	1080	673	22209.	0.	22209.
	FEB 14	42.0	0.0	42.0	1100	685 -	28770•	0.	28770.
	FEB 15	35.0	0.0	35.0	1070	667	23345.	. 0.	23345•
	FEB 16	34.0	0.0	34.0	1060	661	22474•	. 0.	22474.
	FEB 17	36+0	0.0	36.0	1053 (1)	657	23652.	. 0•	23652.
	FEB 18	34.0	0.0	34+0	1047 (1)	653	22202.	0.	22202.
	FEB 19	34.0	0.0	34.0	1040	649	22066.	0.	22066.
	FEB 20	32.0	0.0	32.0	1060	661	21152.	0.	21152.
	FEB 21	31.0	0.0	31.0	1050	655	20305.	0.	20305.
	FEB 22	32.0	0.0	32.0	1050 (1)	655	20960.	0.	20960.
	FE9 23	34.0	0.0	34.0	1050	655	22270. '	0.	22270.
	FE9 24	30.0	0.0	30.0	1050	661	19830.	0.	19830.
	FEB 25	29.0	0.0	29.0	1950	661	19169.	0.	19169.
	FEB 26	36.0	0.0	50∙0	1075 (1)	670	20100.	0.	20100.
	FE9 27	30+0	0.0	30.0	1090	679	20370.	0.	20370.
	FEB 28	44.0	13.8	30+2	1010	631 685*	27764.	7077.	20687.
	TOTAL	. 923.	13.0	909+2		•	615495.	7077.	608418.
HLY	WEIGHTED T.D.S	•				667			

⁽¹⁾ Daily mean E.C. not recorded by U.S.G.S., E.C. estimated by interpolation. *Adjusted T.D.S., for Base Flow, calculated by averaging the T.D.S. on the day before and the day after Storm Flow.

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WEIGHTED T.D.S. CALCULATION SHEET

WATER YEAR 1973-74

T.D.S. = EC 0.000051(EC)+1.549790

Adjusted T.D.S. Times Mean Daily Flow Base U.S.G.S. Storm Flow Flow Mean Daily Total Base U.S.G.S. Mean Storm U.S.G.S. Mean Adjusted T.D.S. Flow Flow Daily Specific Daily Flow F1ow Month-Day Conductance (E.C.) (PPM) (Micromhos) (cfs-Day) (cfs-Day) (cfs-Day) 685 7.7 30.3 1110 691 26258 . 20756+ 5502+ MAR 38.0 685 30.5 756 476 61404. 20893. 98.5 40511. MAR 129.0 685 30.7 794 499 24451. 21030. 18.3 3421. MAR 49.0 3 685 30.8 1070 667 23345. 2247. 21098. 4.7 MAR 35.0 0.0 26.0 960 613 17164. ٥. 17164. MAR 28 0 5 19747. 19747. 0.0 31.0 1020 637 0. MAR 31.0 6 685 989 618 27192+ 5751. 21441. 12.7 31.3 44.0 MAR 685 170 21578. 31.5 266 71570. 389.5 49992. MAR 421.0 685 1050 (1) 655 30130. 21715. 31.7 14.3 8415. MAR 46.0 685 1080 (1) 673 24228. 31.8 21783. 4.2 2445. MAR 10 36.0 691 1110 22112. 0.0 32.0 0. 22112. MAR 11 32.0 673 1080 21536. 0.0 32.0 0. 21536. MAR 32.0 12 1070 667 20677. 0.0 31.0 0. 20677. 31.0 MAR 13 673 0.0 32.0 1080 21536. 0. 21536. MAR 14 32.0 679 0.0 33.0 1090 22407. 0. 22407. MAR 15 33.0 1100 685 22605. 0.0 33.0 0. 22605. MAR 33.0 16 1100 685 21235. 0.0 31.0 0. 21235. MAR 31.0 17 1100 685 21920. 32.0 0.0 0. 21920. MAR 32.0 31.0 1080 673 20863. ٥. 20863. 0.0 MAR 31.0 19 673 29.0 1989 19517. 0.0 ٥. 19517. MAR 20 29.0 1080 673 29.0 19517. 19517. 0.0 ٥. MAR 29.0 21 1060 30.0 661 19830. 0.0 0. 19830. 30.0 MAR 22 1040 649 19470. 30.0 0. 0.0 19470. MAR 30.0 23 1040(1) 649 31.0 20119. 0. 0.0 20119. MAR 24 31.0 1040 649 20766. 0.0 37.0 0. 20768. MAR 25 32.0 1090 679 0.0 32.0 21728. 21728. MAR 26 32.0 1030 643 0.0 33.0 21219. 21219. MAR 27 33.0 1060 661 22474. 0.0 34.0 0. 22474. MAR 28 34.0 664# 1040 649 27258. 8.4 33.6 4948. 22310. MAR 42.0 29 664* 1030 643 27649. 9.9 33.1 5671. 21978. 43.0 MAR 30 664 * 988 617 26531. 32.7 4816. 21713. 10.3 43.0 MAR 31 652719. 786460. 143721. 1552. 578.0 974.0 TOTAL 507

M.W.D. CROSSING

MONTHLY WEIGHTED T.D.S.

Daily mean E.C. not recorded by U.S.G.S., E.C. estimated by interpolation. *Adjusted T.D.S., for Base Flow, calculated by averaging the T.D.S. on the day before and the day after Storm Flow.

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WEIGHTED T.D.S. CALCULATION SHEET

M.W.D. CROSSING WATER YEAR 1973-74

T.D.S. = $\frac{EC}{0.000051(EC) + 1.549790}$

				****			Adjusted T.D	.S. Times Mean	Daily Fl
Month-Day	U.S.G.S. Mean Daily Flow	Storm Flow	Base Flow	U.S.G.S. Mean Daily Specific Conductance (E.C.)	Adjust	Daily sed T.D.S.	U.S.G.S. Total Flow	Storm Fl <i>o</i> w	Base Flow
	(cfs-Day)	(cfs-Day)	(cfs-Day)	(Micromhos)	(PI	<u>M)</u>			
		3.8	32.2	1060	661	664 *	23796.	2415.	21381
APR 1	36+0	45.2	31.8	571	362	664 *	27874.	6759.	21115
APR 2	77.0	5.7	31.3	820(1)	515	590(2)	19055.	588.	18467
APR 3	37.0	5.1	30.9	1070	667	664 ≠	24012.	3494.	20518
APR 4	36.0	3.6	30.4	1040	649	664 *	22066	1880.	20166
APR 5	34.0	0.0	30.0	1070	667	Q Q Q Q Q	20010.	. 0.	20010
APR 6	30.0	0.0	29.0	1060	661		19169.	0.	19169
APR 7	29.0	0.0	27.0	1040	649	-	17523.	. 0.	17523
APR 8	27.0	0.0		1030	643		17361.	0.	17361
APR 9	27.0	0.0	27.0	1040	649		17523.	0.	17523
APR 10	27.0	0.0	27.0	1080	673		17498	0.	17498
APR 11	26.0	0.0	26 • 0 27 • 0	1070	667		18009 •	0.	18009
APR 12	27.0	0.0	26.0	1060	673		17498.	0.	17498
APR 13	26.0	0.0	24.0	1100	685		16440.	0.	1644
APR 14	24.0	0.0	26.0	1100	685		17810.	. O.	17810
APR 15	26.0	0.0		1100	685		17810.	0.	17810
APR 16	26 • 0	0.0	26 • 0 27 • 0	- 1070	667 -		18009	. 0.	18009
APR 17	27.0	0.0		1090	679		17654.	0.	17654
APR 18	26.0	0.0	26+0	1070	667		17342.	0.	1734
APR 19	26.0	0.0	26+0	1070	667		17342.	0.	1734
APR 20	26.0	0.0	26+0	1060	673		17498.	0.	1749
APR 21	26 • 0	0.0	26 • 0	1070	667		17342	0.	1734
APR 22	26+0	0.0	26+0	1080	673		17498	0.	1749
APR 23	26 • 0	0.0	26+0	1087 (1)	677	•	17602.	-0.	1760
APR 24	26.0	0.0	26+0 27+0	1093 (1)	681		18367.	0.	1836
APR 25	27.0	0.0	27.0	1100 (1)	685		18495 •	0.	1849
APR 26	. 27+0	0.0		1102 (1)	686		17836.	0.	1783
APR 27	26.0		26+0	1102 (1)	688		17200•	0.	1720
APR 28	25 • 1	0.0	25.0		690		17940+	0.	1794
APR 29	26.0	. 0.0	26.0	1108 (1)	691		18657	0.	1865
APR 30	27.0	0+0	27.0	1110	. 374				
TOTAL	882.	63.4	818.6	•			562256.	15136.	547120
HTED T.D.S.				•	637				

⁽¹⁾ Daily mean E.C. not recorded by U.S.G.S., E.C. estimated by interpolation.

⁽²⁾ T.D.S. of the Base Flow estimated.

^{*}Adjusted T.D.S., for Base Flow, calculated by averaging the T.D.S. on the day before and the day after Storm Flow.

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WEIGHTED T.D.S. CALCULATION SHEET

WATER YEAR 1973-74

Adjusted T.D.S. Times Mean Daily Flow Base Storm U.S.G.S. Flow Flow. U.S.G.S. Mean Mean Daily Total U.S.G.S. Mean Storm Base Adjusted T.D.S. Flow Daily Specific Flow Daily Flow Flow Month-Day Conductance (E.C.) (PPM) (Micromhos) (cfs-Day) (cfs-Day) (cfs-Day) 673 18171. 18171. ٥. 27.0 27.0 0.0 1080 661 17847. ٥. 17847. 27.0 0.0 27+0 1060 MAY 2 1749B. 673 17498. ٥. 26.0 26.0 1080 MAY 3.0 3 661 17647. ٥. 17847. 27.0 G-Û 27.Ū 1050 MAY 18508. 661 18508. 0. 28.0 MAY 5 28.0 0.0 1060 18676. 667 18676. ٥. 28.0 1070 28.0 0.0 MAY 6 679 19691. 0. 19691. 29.0 0.0 29.0 1090 MAY 7 685 19865. 0. 19865. 0.0 29.0 MAY 29.0 1100 8 679 ٥. 19691. 19691. MAY 29.0 0.0 29.0 1090 9 19348. 691 19348. 0.0 28.0 MAY 10 28.0 1110 19348 . 0. 0.0 28.0 691 19348. MAY 11 28.0 1110 0. 18819. 697 0.0 . 27.0 18819. MAY 12 27.0 1120 691 17966. 0.0 26+0 17966. MAY 13 26.0 1110 17810. 685 17810. MAY 14 26.0 0.0 26.0 1100 685 18495. 18495. 15 27.0 0.0 27.0 1100 MAY 19180. 685 19150. 28.0 1100 MAY 28.0 0.0 16 19180. 685 0. 28.0 19150. MAY 17 28.0 0.0 1100 17654. 0. 679 17654. MAY 0.0 26.0 1090 18 26.0 17495. 673 17496 . 0. 0.0 26.0 MAY 19 26.0 1080 17654. 679 17654. 0. MAY 20 26.0 0.0 26.0 1090 679 18333. 0. 18333. 27.0 0.0 1090 MAY 21 27.0 685 17610. 26.0 17810. 0. 0.0 1100 MAY 22 26.0 679 17654. 0. 23 0.0 26.0 1090 17654. MAY 26.0 17125. 685 0. 17125. MAY 0.0 25.0 1100 24 25.0 685 17810. 0. 17810. 0.0 26.0 MAY 25 26.0 1100 17654. 679 17654. MAY 2ó 0.0 26.0 1090 26.0 17810. 685 17810. MAY 27 0.0 26.0 1100 26.0 18171. 673 18171. 0.0 27.0 1080 MAY 28 27.0 18644. 673 0.0 28.0 1080 18844. MAY 29 28.0 19130. 685 28+0 19180-MAY 0.0 - 1100 30 28.0 17810. 685 17810. 26.0 MAY 31 0.0 1100 26.0 568947. 568947. 837. TOTAL 837. 680 MONTHLY WEIGHTED T.D.S.

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M.W.D. CROSSING

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TABLE NO. E-2

WEIGHTED T.D.S. CALCULATION SHEET

M.W.D. CROSSING

WATER YEAR 1973-74

T.D.S. = $\frac{EC}{0.000051(EC) + 1.549790}$

						Adjusted T.D.	S. Times Mean	Daily Flow
Month-Day	U.S.G.S. Mean Daily Flow	Storm Flow	Base Flow	U.S.G.S. Mean Daily Specific Conductance (E.C.)	Mean Daily Adjusted T.D.S.	U.S.G.S. Total Flow	Storm Flow	Base Flow
	(cfs-Day)	(cfs-Day)	(cfs-Day)	(Micromhos)	(PPM)			
JUN 1	23.0	. 0.0	23.0	1090	679	15617.	0.	15617.
JUN 2	23.0	9.0	23.0	1060	661	15203.	0.	15203.
JUN 3	24.0	0.0	24.0	1060	661	15864.	<u>٠</u>	15864.
JUN 4	25.0	0+0	25.0	1070	667	16675.	Ģ•	16675.
JUN 5	2′ •0	0.0	24.0	1060	661	15864.	0.	15864
JUN 6	24.0	0.0	24.0	1080	673	16152.	. 0•	16152.
JUN 7	24.0	0.0	24.0	1090	679	16296.	0.	16296+
JUN 8	24.0	0.0	24.0	1100	685	16440.	0•	16440.
JUN 9	24.0	0.0	24.0	1090	679	16296•	0.	16296.
JUN 10	23.0	0.0	23.0	1100	685	. 15755•	0.	15755•
JUN 11	23.0	0.0	23.0	1110	691	15893.	0.	15893.
JUN 12	22.0	0.0	22.0	1090	- 679	14938.	• 0•	14938.
JUN 13	21.0	0.0	21.0	1060	661	13881.	0.	13881.
JUN 14	20.0	0.0	20+0	1050	661	13220•	0.	13220.
JUN 15	20.0	0.0	20+0	1060	. 661	13220.	0.	13220•
JUN 16	20.0	0.0	20.0	1060	661	13220•	٥.	13220•
JUN 17	. 21.0	0.0	21.0 ~	- 1070	667 ·	14007.	0.	14007.
JUN 18	22.0	0.0	22.0	1070	667	14674.	0.	14674.
JUN 19	21.0	0.0	21.0	1070	667	14007+	0.	14007.
JUN 20	- 21.0	0.0	21.0	1070	667	14007.	0.	14007. 14007.
JUN 21	21.0	0.0	21.0	1050	655	13755.	0.	13755.
JUN 22	22.0	0.0	22.0	1060	661	14542.	0.	14542•
JUN 23	21.0	0.0	21.0	1060	661	13861.	0.	13861.
JUN 24	21.0	0.0	21.0	1060	661	13861.	0	13861.
JUN 25	21.0	0.0	21.0	1050	655	13755.	0.	13755+
JUN 26	20.0	9+0	20.0	1979	667	13340.	0.	13340+
JUN 27	20.0	0.0	20.0	1070	667	13340.	0.	13340.
JUN 29	20.0	0.0	20.0	- 1080	673	13460.	0.	13460
JUN 29	19.0	0.0	19.0	1090	679	12901	0.	12901.
JUN 30	20.0	0.0	20.0	1090	679	13580.	0.	13580.
TOTAL	654.	0.	654.			437664•	0.	437664.
HTED T.D.S.		•			669		•	

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TABLE NO. E-2

WEIGHTED T.D.S. CALCULATION SHEET

M.W.D. CROSSING

MONTHLY WEIGHTED T.D.S.

WATER YEAR 1973-74

T.D.S. = 0.000051(EC)+1.549790

Adjusted T.D.S. Times Mean Daily Flow U.S.G.S. Storm Base U.S.G.S. Mean Mean Daily Total Flow Flow Storm Base U.S.G.S. Mean Adjusted T.D.S. Flow. Flow Flow. Daily Specific Month-Day Daily Flow Conductance (E.C.) (PPM) (cfs-Day) (cfs-Day) (cfs-Day) (Micromhos) 691 14511. 0. 14511. 0.0 21.0 1110 21.0 JUL 1 691 13820 • 0. 13820. 0.0 20.0 1110 JUL 2 20.0 697 13940+ 0 . 13940. 0.0 20.0 1120 JUL 20.0 13940. ٥. 13940 . 697 0.0 20.0 1120 JUL 20+0 Ţ 13700. ٥. 13700. 685 0.0 20.0 1100 JUL 21.0 13700. 0. 13700 . 685 0.0 20.0 1100 JUL 6 20.0 13700. 13700. 685 0+0 20.0 1100 JUL 20.0 13700 . 0. 13700 -685 0.0 20.0 1100 JUL 20.0 13700. 0. 13700. 685 0.0 20.0 1100 JUL 20.0 9 . 13580. 0. 13580-679 0.0 20.0 1090 JUL 10 20.0 679 13580. 0. 13580. 0.0 20.0 1090 JUL 11 20.0 679 13560. 0. 13580. 0.0 20.0 1090 20.0 JUL 12 679 13560. 0. 13560 · 0.0 20.0 1090 JUL 20.0 13 13580. 0. 0.0 679 13580. 20.0 1090 JUL 20.0 14 13820. 0. 20.0 691 13820. 0.0 1110 JUL 20.0 15 12901. 679 ٥. 12901. 0.0 19.0 1090 JUL 16 19.0 673 12787. 12787. 0.0 19.0 1080 JUL 17 19.0 12787. ٥. 12787. 19.0 0.0 JUL 19.0 1080 18 685 13015. ٥. 13015. 0.0 19.0 1100 JUL 19 19.0 685 13015. ٥. 13015. 0.0 19.0 1100 JUL 20 19.0 13015. 0. 13015. 685 19.0 1100 JUL 21 19.0 685 13015+ 0. 13015. 19.0 0.0 1100 JUL 22 19.0 13129. 13129. 19.0 691 ٥. 0.0 JUL 19.0 1110 23 13015. 685 0. 13015. 0.0 19+0 JUL 1100 24 19.0 12222. 12222. 679 ٥. 0.0 18.0 1090 JUL 18.0 25 685 12333. 0. 12330. 0.0 18.0 1100 JUL 26 18.0 12330. 12330. 685 ٥. 0.0 18.0 1100 18.0 JUL 27 673 12114. 12114. 18.0 0.0 1080 18.0 JUL 28 12330. ٥. 685 12330. 18.0 1100 0.0 18.0 JUL 29 13243. 697 ٥. 13243. 19.0 1120 0.0 JUL 19.0 30 673 12787. 0. 12787. 0.0 19.0 1090 JUL 31 19.0 410466. 410466. 600. TOTAL 600. 684

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TABLE NO. E-2

WEIGHTED T.D.S. CALCULATION SHRET

WATER YEAR 1973-74

0.000051(EC)+1.549790

Adjusted T.D.S. Times Mean Daily Flow U.S.G.S. Storm Base U.S.G.S. Mean U.S.G.S. Mean Storm Base Mean Daily Total Flow Flow Month-Day Daily Flow Flow Flow Daily Specific Adjusted T.D.S. Flow. Conductance (E.C.) (cfs-Day) (cfs-Day) (cfs-Day) (Micromhos) (PPM) 1 2 19.0 19.0 0.0 1080 673 12767. 12787. AUG 0.0 18.0 1070 18.0 667 12006. 12006. AUG 3 18.0 18.0 0.0 1100 665 12330. ٥. 12330. AUG 18.0 0.0 18.0 1100 685 12330 . û. 12330. AUG 5 0.0 18.0 1090 E 18.0 679 12222. 0. 12222. AUG 0.0 20.0 1090 20.0 679 13560. ٥. 13560. AUG 18.0 0.0 18.0 1110 12 691 12438. Ō. 12438. AUG 18.0 0.0 18.0 1090 679 12222. 12222. AUG 9 18.0 18.0 1050 573 12114. 0. 12114. AUS 10 18.0 18.0 1060 661 11898. ٥. 11898. AUG 11 19.0 0.0 19.0 1080 673 12767. ٥. 12767. AUG 12 0.0 18.0 1090 18.0 679 12222. 0. 12222. AUG 13 19.0 19.0 0.0 1100 685 13015. 0. 13015. AUG 14 19.0 0.0 19.0 1090 679 12901. 12901. AUG 15 18.0 18.0 0.0 1100 685 12330. 12330. AUG 18.0 18.0 0.0 1100 685 12330. 12330. AUG 19.0 0.0 18.0 1110 691 12438. ٥. 12436 . AUG 18 18.0 0.0 18.0 1120 697 12546. 0. 12546. AUG 19 18.0 0.0 18.0 1110 691 12438 . ٥. 12438 . AUG 20 18.0 0.0 18.0 1110 691 12438 . 0. 12438. AUG 21 18.0 18.0 1110 691 12438. 0. 12438. AUG 22 18.0 1130 18+0 0.0 703 12654. 0. 12654. AUG 23 19.0 1130 19.0 0.0 703 13357. 0. 13357. AUG 24 18.0 18.0 0.0 1120 697 12546. 0. 12546. AUG 25 18.0 18.0 1110 0.0 691 12438. 12438. AUG 26 18.0 0.40 12.0 1110 691 12458 . 12438. AUG 27 18.0 18.0 1100 0.0 685 12330. 0. 12330. AUG 28 18.0 1120 15.0 0.0 697 12546. 0. 12546. AUG 29 18.0 0.0 18.0 1130 703 12654. 0. 12654. AUG 30 18.0 0.0 18.0 1110 691 12438. ٥. 12438 -AUG 31 19.0 0.0 19.0 1110 691 13129. 13129. 0. 566. 0. 388340. 388340. MONTHLY WEIGHTED T.D.S.

686

M.W.D. CROSSING

age 12 of 12

WEIGHTED T.D.S. CALCULATION SHEET

M.W.D. CROSSING

WATER YEAR 1973-74

T.D.S. = $\frac{EC}{0.000051(EC)+1.549790}$

		-				Adjusted T.D	.S. Times Mean	Daily Flo
Month-Day	U.S.G.S. Mean Daily Flow	Storm Flow	Base Flow	U.S.G.S. Mean Daily Specific Conductance (E.C.)	Mean Daily Adjusted T.D.S.	U.S.G.S. Total Flow	S torm Flow	Base Flow
	(cfs-Day)	(cfs-Day)	(cfs-Day)	(Micromhos)	(PPM)			· .
SEP 1	18.0	0.0	18.0	. 1090	679	12222•	. 0.	12222.
SEP 2	19.0	0.0	19.0	· 1090	679	12901•	0.	12901.
SEP 3	18.0	0.0	18.0	1100	685	12330.	0.	12330.
SEP 4	18 = C	0.0	18.0	1090	679	12222:	Q e	12222.
SEP 5	18.0	0.0	13.0	1090	679	12222•	0.	12222.
SEP 6	18.0	0.0	18.0	1070	667	12006 •	0+	12006
SEP 7	18.0	0.0	18.0	1070	667	12006.	0.	12006
SEP 8	18.0	0.0	18.0	1070	667	12006.	Q.	12006
SEP 9	17.0	0.0	17.0	1090	679	11543.	0.	11543
SEP 10	17-0	0.0	17.0	1060	661	11237.	0.	11237
SEP 11	18.0	0.0	18.0	1070	667	12006.	0.	12006
SEP 12	18.0	0.0	. 18.0	1060	661	11898.	G'.	11898
SEP 13	18.0	0.0	18.0	1050	655	11790.	0.	11790
SEP 14	18.0	0.0	18.0	1060	661 ⁻	11898.	0•	11898
SEP 15	18.0	0.0	18.0	1065 (1)	664	11952.	0.	11952
SEP 16	18.0	0.0	18.0	1070 (1)	667	12006.	0.	12006
SEP 17	18.0	0.0	18.0 -	1075 (1)	670	12060.	0.	12060
SEP 18	18+0	0.0	18.0	1080	673	12114.	0.	12114
SEP 19	18.0	0.0	18.0	1120	697	12546.	0.	12546
SEP 20 -	19+0	0.0	19 • C	1100	685	13015	Q.	13015
SEP 21	19.0	0.0	19+0	1100 .	685	13015.	O• ·	13015
SEP 22	18.0	0.0	18.0	1100	685	12330.	0.	12330
SEP 23	18.0	0.0	18.0	1090	679	12222.	0.	12222
5EP 24	18.0	0.0	18.0	1090	679	12222• `	0.	12222
SEP 25	18.0	0+0	18.0	1090	679	12222.	0.	12222
SEP 26 .	18-0	0.0	18.0	1100	685	12330.	0.	12330
SE2 27	18.0	0.0	18+0	1100	685	12330.	٥.	12330
5EP 28	18.0	0.0	18.0	1100	685	12330.	0.	12330
5EP 29	18.0	0.0	18.0	1100	685	12330.	0.	12330
SEP 30	18.0	0.0	18.0	1120	697	12546.	0.	12546
TOTAL	541.	0•	541.			365857.	0.	365857
HTED T.D.S.					676			

⁽¹⁾ Daily mean E.C. not recorded by U.S.G.S., E.C. estimated by interpolation.

SUMMARY

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WATER QUALITY FOR THE RIVERSIDE NARROWS

METROPOLITAN WATER DISTRICT (MWD) CROSSING

WATER YEAR 1973-74

		Mean	Daily Flow		Monthly Weighted	2	an Daily Fl Adjusted T	
M	onth	U.S.G.S. Total Flow (cfs-Days)	Storm Flow (cfs-Days)	Base Flow (cfs-Days)	Average Adjusted T.D.S. (ppm)	U.S.G.S. Total Flow	Storm Flow	Base Flow
973	October	634	0.0	634	676	428,818	0	428,818
	November	866	211.0	655.0	652	564,801	129,419	435,382
-	December	723	4.0	719.0	672	485,501	2,632	482,869
1974	January	4,075	3,267.0	808.0	360	1,476,868	932,586	544,282
	February	923	13.8	909.2	667	615,495	7,077	608,418
	March	1,552	578.0	974.0	494	786,460	133,721	652,739
	April	882	63.4	818.6	637	562,256	15,136	547,120
	May	837	0.0	837	680	568,947	0	568,947
	June	654	0.0	654	669	437,664	0	437,664
	July	600	0.0	600	684	410,466	. 0	410,466
	August	566	0.0	566	686	388,340	0	3 88,340
	September	541	0.0	541	676	365,857	0	3 65,857
- <u></u>	Total	12,853	4,137.2	8,715.8		7,091,473	1,220,571	5,870,902
otal	A.F.	25,494	8,206	17,288				

Weighted Average Annual (Base Flow) T.D.S. 674 ppm

Weighted Average Annual (Storm Flow) $\frac{1220571}{4137.2}$ T.D.S. = 295 ppm

Weighted Average Annual (Total Flow) T.D.S. 7091473 552 ppm 12853

U.S.G.S. WATER QUALITY SAMPLES RIVERSIDE QUALITY CONTROL PLANT WATER YEAR 1973-74

•	WITH THAT INT	7
Date	E.C.	T.D.S.
1973 October	972	587
•	968	569
	1100	626
	1020	575
November	1060	599
	1040	603
	1040	603
	909 .	- 505
December	925	530
	950	538
	910	483
107/ Tonuowa	850 855	485
1974 January	855 848	503
	969	554
February	911	529
repluary	1190 1200	, 783
	1230	667
,	1300	692
March	1110	723
Imicii	1180	609 633
	1110	589
	1030	579
April	1210	700
white	1200	704
	1290	519
	1170	692
May	1230	728
	980	584
	1010	600
	1120	631
,	1080	639
June	1120	650
7	1100	647
	1180	695
	1240	735
July	1140	686
•	1120	678
	1110	685
	1110	675
August	1130	697
	1100	674
•	1100	664
	1140	682
•	1160	692
September	1110	673
	1110	678
	1140	702
	1120	680

WEIGHTED T.D.S. CALCULATION SHEET

RIVERSIDE QUALITY CONTROL PLANT

WATER YEAR 1973-1974 TDS=EC/(0.000046(EC)+ 1.679334)

	MONTH-DAY	U.S.G.S. MEAN Daily flow	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (E.C.)	MEAN DAILY ADJUSTED T.D.S.	MEAN DAILY FLUW TIMES ADJUSTED T.D.S.
		(CFS-DAY)	(MICROMHOS)	(PPM)	
	OCT 1	27.0	1040	602	16254•
	· OCT 2	27•0	1020	591	15957.
	OCT 3	27.0	1020	591	15957.
	OCT 4	27.0	1080	625	16875.
	OCT 5	28.0	1050	608	17024.
	OCT 6	26.0	1080	625	16250•
	OCT 7	25.0	1010	585	14625.
	ОСТ В	28.0	979	568	15904.
	OCT 9	28.0	998	578	16164.
	OCT 10	27.0	999	579	15633.
	OCT 11	27.0	1020	591	15957•
	OCT 12	27.0	1100	636	17172.
	OCT 13	26.0	1100	636	16536.
Ħ	OCT 14	26.0	1040	602	15652•
l	OCT 15	28.0	1060	613	17164.
16	OCT 16	28.0	1090	630	17640.
-	OCT 17	27.0	1080	625	16875.
	OCT 18	28.0	1110	641	17948.
	OCT 19	28.0	1120	647	18116.
	OCT 20	26.0	1120	647	16822.
	OCT 21	24.0	1070	619	14856.
	OCT 22	28.0	1040	602	16856.
	OCT 23	28.0	1070	619	17332.
	OCT 24	27.0	1050	608	16416.
	OCT 25	27.0	1020	591	15957.
	OCT 26	27.0	1060	613	16551.
	OCT 27	26.0	1060	613	15938.
	OCT 28	26.0	1040	602	15652.
	OCT 29	28.0	1040	602	16856.
	OCT 30	27.0	1100	636	17172.
	OCT 31	27.0	1070	619	16713.

836.

TOTAL MONTHLY WEIGHTED T.D.S.

WEIGHTED T.D.S. CALCULATION SHEET

RIVERSIDE QUALITY CONTROL PLANT

WATER YEAR 1973-1974 TDS=EC/(0.000046(EC)+ 1.679334)

	MONTH-DAY	U.S.G.S. MEAN DAILY FLOW	U.S.G.S. MEAN DAILY SPECIFIC	MEAN DAILY ADJUSTED T.D.S.	MEAN DAILY FLOW TIMES
		(CFS-DAY)	CONDUCTANCE (E.C.) (MICROMHOS)	(PPM)	ADJUSTED T.D.S.
	NOV 1	28 • 0	1090	630	17640•
	NOV 2	28.0	1090	630	17640.
	NOV 3	26.0	1090	630	16380.
	NOV 4	25.0	1020	591	14775.
	NOV 5	28.0	1138	657	18396.
	NOV 6	27.0	1120	647	17469.
	NOV 7	. 27.0	1060	613	16551.
	NOV 8	28.0	1030	597	16716.
	NOV 9	28.0	1050	608	17024.
	NOV 10	26.0	1030	597	15522•
	NOV 11	26.0	1010	585	15210.
	NOV 12	28.0	1070	619	17332.
	NOV 13	28.0	1140	658	18424.
н	NOV 14	27.0	1110	641	17307•
E-17	NOV 15	27.0	1060	613	16551.
17	NOV 16	27.0	1050	608	16416.
	NOV 17	26.0	1060	613	15938.
	NOV 18	28.0	965	560	15680.
	NOV 19	28.0	921	535	14980.
	NOV 20	27.0	1000	580	15660•
	NOV 21	27.0	1020	591	15957.
	NOV 22	23.0	974	565	12995.
	NOV 23	24•0	926	538	12912.
	NOV · 24	24.0	960	557	13368.
	NOV 25	25•0	970	563	14075.
	NOV 26	27.0 ·	891	518	13986.
	NOV 27	26.0	909	528	13728.
	NOV 28	26.0	919	534	13884.
	NOV 29	26.0	949	. 551	14326.
	NOV 30	26.0	941	546	14196.
	TOTAL	797.	•		471038.

MONTHLY WEIGHTED T.D.S.

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WATER YEAR 1973-1974 TDS=EC/(0.000046(EC)+ 1.679334)

WEIGHTED T.D.S. CALCULATION SHEET

RIVERSIDE QUALITY CONTROL PLANT

MONTHLY WEIGHTED T.D.S.

	MONTH-DAY	U.S.G.S. MEAN DAILY FLOW	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (E.C.)	MEAN DAILY ADJUSTED T.D.S.	MEAN DAILY FLOW TIMES ADJUSTED T.D.S.
		(CFS-DAY)	(MICROMHOS)	(PPM)	
	DEC 1	24•0	918	533	12792.
	DEC 2	25.0	880	512	12800•
	DEC 3	28.0	888	516	14448.
	DEC 4	27.0	908	528	14256.
	DEC 5	26.0	906	526	13676.
	DEC 6	27.0	909	528	14256.
	DEC 7	26.0	872	507	13182.
	DEC 8	26.0	880	512	13312.
	DEC 9	23.0	868	505	11615.
	DEC 10 .	26•0	940	546	14196•
	DEC 11	26.0	929	539	14014.
	DEC 12	26.0	926	538	13988.
	DEC 13	26.0	936	543	14118.
	DEC 14	26.0	953	553	14378.
· 卢	DEC 15	26•0	948	550	14300•
1	DEC 16	25 • 0	917	533	13325.
18	DEC 17	27.0	917	533	14391.
	DEC 18	26 • 0	927	538	13988.
	DEC 19	26.0	914	531 .	13806.
	DEC 20	26.0	939	545	14170•
	DEC 21	26.0	941	546	14196.
	DEC .22	24.0	932	541	12984.
	DEC 23	23.0	909	528	12144.
	DEC 24	24.0	926	538	12912.
	DEC 25	21.0	914	531	11151.
	DEC 26	23.0	897	521	11983.
	DEC 27	24.0	963	55 9	13416.
	DEC 28	24.0	1030	597	14328•
	DEC 29	23.0	1010	585	13455•
	DEC 30	22.0	997	578	12716.
	DEC 31	25.0	927	538	13450.
	TOTAL	777.0			417746.

WEIGHTED T.D.S. CALCULATION SHEET

RIVERSIDE QUALITY CONTROL PLANT WATER YEAR 1973-1974 TDS=EC/(0.000046(EC)+ 1.679334)

	MONTH-DAY	U.S.G.S. MEAN DAILY FLOW	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (E.C.)	MEAN DAILY ADJUSTED T.D.S.	MEAN DAILY FLOW TIMES ADJUSTED T.D.S.
		(CFS-DAY)	(MICROMHOS)	(PPM)	
	JAN 1	21.0	87 9	511	10731•
	JAN 1 JAN 2	25.0	922	536	13400•
	JAN 3	25.0	982	569	14225.
	JAN 4	28.0	947	550	15400.
	JAN 5	26.0	870	506	13156.
	JAN 6	24.0	960	. 557	13368.
	JAN 7	31.0	906	526	16306.
	JAN 8	30.0	917	533	15990•
	JAN 9	27.0	1040	602	16254.
	JAN 10	27.0	1070	619	16713.
	JAN 11	27.0	1060	613	16551•
	JAN 12	26.0	1080	625	16250•
	JAN 13	26.0	1050	608	15808.
西	JAN 14	26.0	999	579	15054.
• ⊢	JAN 15	27.0	1030	597	16119.
19	JAN 16	27.0	1030	597	16119.
	JAN 17	27.0	1010	585	15795•
	JAN 18	27.0	980	568	15336.
	JAN 19	25.0	978	567	14175.
	JAN 20	25.0	946	549	13725•
	JAN 21	27.0	937	544	14688.
	JAN 22	26.0	967	561	14586.
	JAN 23	26.0	991	575	14950.
	JAN 24	27.0	1030	597	16119.
	JAN 25	26.0	1100	636	16536•
	JAN 26	26.0	1090	630	16380.
	JAN 27	25.0	1080	625	15625•
	JAN 28	26.0	1090	630	16380.
	JAN 29	26.0	1150	664	17264.
	JAN 30	26.0	1120	647	16322.
	JAN 31	27.0	1140	658	17766.

TOTAL MONTHLY WEIGHTED T.D.S. 815.0

477591.

WEIGHTED T.D.S. CALCULATION SHEET

RIVERSIDE	QUALITY C	ONTROL	PLANT WATER	YEAR	1973-1974	TDS=EC/(0.000046(EC)+	1.6793341
	MONTH-DA	Y	U.S.G.S. MEAN DAILY FLOW		U.S.G.S. MEA DAILY SPECIFI CONDUCTANCE (E	IC A	MEAN DAILY DJUSTED T.D.S.	MEAN DAILY FLOW TIMES ADJUSTED T.D.S.
			(CFS-DAY)		(MICROMHOS)		(PPM)	
		1	26•0		1110		641	16656.
		2	25.0		1080		625	15625•
		3	23.0		1040		602	13846.
		4	27.0		1050		608	16416.
	FEB	5	26.0		1150		664	17264.
		6	26.0		1240		714	18564•
		7	. 26.0		1260		725	18850•
		8	26.0		1220		703	18278•
	FEB	9	25.0		1210		697	17425•
	FEB 1	0	23.0		1150		664	15272•
	FEB 1	1	26.0		1150		664	17264.
	FEB 1	2	26.0		1190		686	17836.
	FEB 1		26.0		1240		714	18564.
王-20	FEB 1	4	26.0		1260		725	18850•
-2	FE9 1	5	26.0		1200		692	17992.
. 0	FEB 1		27.0		1180		681	18367.
	FEB 1		23.0	•	1140		658	15134.
	FEB 1	8	27.0		1190		686	18522•
	FEB 1	9	26.0		1210		697	18122.
	FEB 2	0	26.0		1250	a en	720	18720.
	FEB 2		26.0		1270		731	19006.
	FEB 2		26.0		1230		709	18434.
	FEB 2		25.0	•	1230	•	709	17725.
	FEB · 2		24.0		1130		653	15672.
	FE8 2		28.0		1130		653	18284.
	FEB 2		26 • 0	*	1210		697	18122.
	FEB 2		26.0		1360		781	20306.
	FEB 2		26.0		1360		781	20306.
	TOTAL		719.					495452.
MONTHLY WE	IGHTED Tel	D.S.					689	

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TABLE NO. E-5

WEIGHTED T.D.S. CALCULATION SHEET

RIVERSIDE QUALITY CONTROL PLANT WATER YEAR 1973-1974 TDS=EC/(0.000046(EC)+ 1.679334)

	MONTH-DAY	U.S.G.S. MEAN Daily flow	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (E.C.)	MEAN DAILY ADJUSTED T.D.S.	MEAN DAILY FLOW TIMES ADJUSTED T.D.S.
		(CFS-DAY)	(MICROMHOS)	(PPM)	
	MAR 1	27.0	1200	692	18684.
	MAR 2	27.0	1140	658	17766•
	MAR 3	25.0	1160	669	16725•
	MAR 4	27.0	1160	669	18063.
	MAR 5	27.0	1140	658	17766.
	MAR 6	27.0	1150	664	17928•
	MAR 7	26.0	1150	664	17264.
	MAR 8	28.0	1090	630	17640.
	MAR 9	26•0	1140	658	17108.
	MAR 10	25.0	1170	675	16875.
	MAR 11	28.0	1200	692	19376.
	MAR 12	<u>2</u> 7•0	1150	664	17928.
	MAR 13	27.0	1120	647	17459.
	MAR 14	27.0	1100	635	17172•
দ্ৰ	MAR 15	27.0	1050	608	16416.
2	MAR 16	25.0	1030	597	14925•
_	MAR 17	24.0	1040	602	14448•
	MAR 18	26.0	1070	619	16094•
	MAR 19	29.0	1070	619	17951.
	MAR 20	26.0	1140	658	17108.
	MAR 21	27.0	1110	641	17307•
	MAR .22	27.0	1160	669	18063.
	MAR 23	26.0	1100	636	16536.
	MAR · 24	25.0	1020	591	14775.
	MAR 25	27.0	1010	585	15795•
	MAR 26	28.0	1070	619	17332•
	MAR 27	27.0	1040	602	16254.
	MAR 28	27.0	1040	602	16254.
	MAR 29	27.0	1030	597	16119.
	MAR 30	26.0	982	569	14794.
	MAR 31	24.0	932	541	12984.

TOTAL
MONTHLY WEIGHTED T.D.S.

822.0

634

WEIGHTED T.D.S. CALCULATION SHEET

RIVERSIDE	QUALITY	CONTROL	PLANT	WATER	YEAR	1973-1974	TDS=EC/(0.000046(EC)+	1.679334)
	MONTH-	DAY		S. MEAN		U.S.G.S. ME DAILY SPECIF ONDUCTANCE	FIC AD	MEAN DAILY JUSTED T.D.S.	MEAN DAILY FLOW TIMES ADJUSTED T.D.S.
		·	(CFS	S-DAY)		(MICROMHOS		(PPM)	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
	APR	1		27.0		987		572	15444•
	APR	2		28.0		1060		613	17164.
	APR	3		28.0		1140		658	18424•
	APR	4		27.0		1230		709	19143.
	APR	5		27.0		1220	*	703	18981•
	APR	6		26.0		1160		669	17394•
	APR	7		25.0		1140		658	16450•
	APR	8	· :	28.0		1190		686	19208.
	APR	9	•	26.0		1260		725	18850•
	APR	10		28.0		1280		736	20608•
	APR	11		28.0		1250	* ***	720	20160.
	APR	12		27.0		1270		731	19737•
	APR	13		26.0		1210		697	18122•
tبا	APR	14		23.0		1240		714	16422•
1	APR	15		27.0		1340		770	20790.
.22	APR	16		26.0		1370		786	20436.
	APR	17		26.0	100	1290	•	742	19292•
	APR	18		27.0		1240		714	19278•
	APR	19		27.0		1300		747	20169•
	APR	20		25.0		1260	and the second of the second o	725	18125•
	APR	21		25.0		1200		692	17300.
				28.0		1170		675	18900•
		. 22 23		27.0	i	1240	Annual Control of the Control	714	19278•
	APR					1290		742	20776.
	APR'	24		28.0				686	19894•
	APR	25		29.0		1190	· · · · · · · · · · · · · · · · · · ·	697	18819.
	APR	26		27.0		1210			17550.
	APR	27		26.0		1170		675	16600.
	APR	28		25.0		1150		664	
	APR	29		28.0	•	1140		658	18424•
	APR	30		28.0		1200		692	19376.
	то	TAL		803.			·		561114.

MONTHLY WEIGHTED T.D.S.

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TABLE NO. E-5 Page 8 of .

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WEIGHTED T.D.S. CALCULATION SHEET

RIVERSIDE QUALITY CONTROL PLANT WATER YEAR 1973-1974 TDS=EC/(0.000046(EC)+ 1.679334)

•	MONTH-	DAY	U.S.G.S. MEAN Daily flow	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (E.C.)	MEAN DAILY ADJUSTED T.D.S.	MEAN DAILY FLOW TIMES ADJUSTED T.D.S.
. '			(CFS-DAY)	(MICROMHOS)	(PPM)	
	MAY	1	28.0	1280	736	20608•
	MAY	2	28.0	1200	692	19376•
	MAY	3	28.0	1200	692	19376.
	MAY	4	26.0	1100	636	16536.
	MAY	5	25.0	1010	585	14625.
-	MAY	6	28.0	978	567	15876•
	MAY	7	. 28.0	958	556	15568•
	MAY	8	28.0	990	574	16072•
	MAY	9	30.0	1040	602	18060•
	MAY	10	30.0	1100	636	19080.
	MAY	11	29•0	983	570	16530•
	MAY	12	28.0	914	531	14868.
	MAY	13	30.0	933	542	16260.
Ħ	MAY	14	29.0	974	565	16385•
1	MAY	15	30.0	1010	585	17550•
. 23	MAY	16	30.0	1010	585	17550.
	MAY	17	30.0	981	569	17070•
	MAY	18	28.0	981	569	15932∙
	MAY	19	27.0	972	564	15228•
	. MAY	20	30.0	986	572	17160.
	MAY	21	27.0	1040	. 602	16254.
	MAY	22	28.0	1140	658	18424.
	MAY	23	28.0	1130	653	18284.
	MAY	24	30.0	1170	675	20250.
	MAY	25	27.0	1180	681	18387.
	MAY	26	25.0	1110	641	16025.
	MAY	27	27.0	1120	647	17469.
	MAY	28	28.0	1150	664	18592.
	MAY	29	27.0	1170	675	18225.
	MAY	30	29.0	1120	647	18763.
	MAY	31	29.0	1160	669	19401.

TOTAL MONTHLY WEIGHTED T.D.S.

875.

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WEIGHTED T.D.S. CALCULATION SHEET

RIVERSIDE QUALITY CONTROL PLANT

WATER YEAR 1973-1974 TDS=EC/(0.000046(EC)+ 1.679334)

	MONTH-DAY	U.S.G.S. MEAN DAILY FLOW	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (E.C.)	MEAN DAILY ADJUSTED T.D.S.	MEAN DAILY FLOW TIMES ADJUSTED T.D.S.
		(CFS-DAY)	(MICROMHOS)	(PPM)	
	JUN 1	27.0	1110	641	17307•
	JUN 2	27.0	1050	608	16416.
	JUN ' 3	29.0	1060	613	17777•
	JUN 4	29.0	1100	636	18444.
	JUN 5	30.0	1150	664	19920•
	JUN 6	29.0	1160	669	19401.
	JUN 7	. 29•0	1110	641	18589•
	8 //UL	29•0	1070	619	17951•
	9 אטע	27.0	1010	585	15795•
	JUN 10	30.0	1050	608	18240•
	JUN 11	29•0	1100	, 636	18444•
	JUN 12	30.0	1080	625	18750•
	JUN 13	31.0	1080	625	19375.
Ħ	JUN 14	31.0	1110	641	19871.
E-2	JUN 15	29.0	1140	658	19082•
4.	JUN 16	28.0	1080	625	17500•
	JUN 17	31.0	1160	669	20739•
	JUN 18	31.0	1160	669	20739•
	JUN 19	30∙0	1170	675	20250•
	. JUN 20	29.0	1180	681	19749•
	JUN 21	30.0	1180	681	20430•
	JUN 22	28.0	1120	647	18116.
	JUN 23	26.0	1060	613	15938•
	JUN · 24	29•0	1110	641	18589•
	JUN 25	29.0	1220	703	20387•
	JUN 26	29.0	1260	725	21025•
,	JUN 27	28.0	1260	7 25	20300•
	JUN 28	28.0	1260	725	20300•
	92 NUL	27.0	1280	736	19872•
	JUN 30	25.0	1240	714	17850.
	TOTAL	864.	·	•	567146.

MONTHLY WEIGHTED T.D.S.

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WEIGHTED T.D.S. CALCULATION SHEET

RIVERSIDE QUALITY CONTROL PLANT WATER YEAR 1973-1974 TDS=EC/(0.000046(EC)+ 1.679334)

	MONTH-DAY	U.S.G.S. MEAN DAILY FLOW (CFS-DAY)	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (E.C.) (MICROMHOS)	MEAN DAILY ADJUSTED T.D.S. (PPM)	MEAN DAILY FLOW TIMES ADJUSTED T.D.S.
		(CIO DAI)	til Champay	** 1 1-10	
	JUL 1	28.0	1160	669	18732.
	JUL 2	27.0	1170	675	18225•
	JUL 3	27.0	1140	658	17766.
	JUL 4	27.0	1200	692	18684.
	JUL 5	29•0	1170	675	19575.
	JUL 6	27.0	1130	653	17631.
	JUL 7	. 26.0	1120	647	16822.
	JUL 8	29•0	1130	653	18937.
	JUL 9	29•0	1190	686	19894•
•	JUL 10	28•0	1220	703	19684.
	JUL 11	28.0	1120	647	18116.
	JUL 12	28 • 0	. 1130	653	18254.
	JUL 13	26∙0	1150	664	17264.
Ħ	JUL 14	25•0	1140	658	16450•
. 2	JUL 15	29•0	1120	647	18763.
່ີທີ	JUL 16 '	28•0	1150	664	18592•
	JUL 17	27.0	1190	686	18522•
	JUL 18	27.0	1180	681	18387•
	JUL 19	28.0	1190	686	19208 •
	JUL 20	27.0	1200	692	18684.
	JUL 21	- 24•0	1170	675	16200•
	JUL 22	27.0	1160	669	18063.
	JUL 23	27.0	1170	675	18225•
	JUL · 24	27.0	1220	703	18981.
	JUL 25	27.0	1190	686	18522.
	JUL 26	28.0	1200	692	19376.
	JUL 27	25.0	1210	697	17425•
	JUL 28	25.0	1170	675	16875.
	JUL 29	28.0	1160	669	18732.
	JUL 30	29.0	1200	692	20068•
	JUL 31	27.0	1180	681	18387.

MONTHLY WEIGHTED T.D.S.

844.

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576532.

WEIGHTED T.D.S. CALCULATION SHEET

RIVERSIDE	QUALITY	CONTROL	PLANT	WATER	YEAR	1973-1974	TDS=EC/	0.000046(EC)+	1.679334)
	MONTH-	DAY		•S• MEAN Y FLOW		U.S.G.S. ME DAILY SPECIF CONDUCTANCE	FIC A	MEAN DAILY	MEAN DAILY FLOW TIMES ADJUSTED T.D.S.
			(CF	S-DAY)		(MICROMHO		(PPM)	
	AUG	1		29.0		1170		675	19575.
	AUG	2		30.0		1180		681	20430•
	AUG	3		27•Ó		1160		669	18063.
	AUG	4		26.0		1140		658	17108.
•	AUG	5	4	30.0		1140		658	19740•
	AUG	6		29.0		1140		658	19082•
	AUG	7		29.0		1140		658	19082•
	AUG	8		29.0		1140	*	658	19082•
	AUG	9	•	28.0		1180		681	19068•
	AUG	10		27.0		1180		681	18387•
	AUG	11		26.0		1130		653	16978.
	AUG	12		29.0		1110		641	18589•
	AUG	13		29.0		1140		658	190 <i>5</i> 2•
Ħ	AUG	14		28.0	•	1130		653	18284•
1	AUG	15	-	29.0		1130		653	18937.
26	AUG	16		29.0		1140		658	19082.
	AUG	17		27.0		1150		664	17928•
	AUG	18		26.0		1120		647	16822•
	AUG	19		29.0		1140		658	19082.
	AUG	20		28.0		1150		664	18592•
	AUG	21		28.0		. 1150		664	18592.
	AUG	.22		28.0		1140		658	18424•
	AUG	23	•	28.0		1160	and the second second	669	18732•
	AUG '	24		27.0		1150		664	17928.
	AUG	25		26.0		1110		641	16566.
	AUG	26	٠	29.0	*	1110		641	18589.
	AUG	27		28.0		1160		669	18732.
	AUG	28		28.0		1170		675	18900•
	AUG	29	•	29.0		1190		686	19894.
	AUG	30		28.0		1200		692	19376.
	AUG	31		26.0		1180	•	681	17706.

869.

MONTHLY WEIGHTED T.D.S.

WEIGHTED T.D.S. CALCULATION SHEET

RIVERSIDE QUALITY CONTROL PLANT

WATER YEAR 1973-1974 TDS=EC/(0.000046(EC)+ 1.679334)

	MONTH-D	PAY	U.S.G.S. MEAN DAILY FLOW (CFS-DAY)	U.S.G.S. MEAN DAILY SPECIFIC CONDUCTANCE (E.C.) (MICROMHOS)	MEAN DAILY ADJUSTED T.D.S. (PPM)	MEAN DAILY FLOW TIMES ADJUSTED T.D.S.
			(CI 3-DAI)	(MICROMHOS)	(PPM)	
	SEP	1	24.0	1090	630	15120•
	SEP	2	26.0	1070	619	16094.
	SEP	3	28.0	1120	647	18116.
	SEP	4	29.0	1150	664	19256.
	SEP	5	28.0	1150	664	18592.
	SEP	6	29.0	1250	720	20880.
	SEP	7	27.0	1170	675	18225.
	SEP	8	26.0	1100	636	16536.
	SEP	9	29.0	1100	636	18444.
	SEP	10	29.0	1130	653	18937.
	SEP	11	29.0	1150	664	19256.
	SEP	12	29+0	1150	664	19256.
	SEP	13	29.0	1160	669	19401.
H	SEP	14	27.0	1100	636	17172.
-27	SEP	15	26.0	1050	608	15808.
7	SEP	16	29.0	1060	613	17777.
•	SEP	17	29.0	1150	664	19256.
	SEP	18	29.0	1150	664	19256.
		19	29.0	1130	` 653	18937.
		20	29.0	1120	647	18763.
	SEP	21	27.0	1110	641	17307.
	SEP .	22	27.0	1100	636	17172.
		23	30.0	1110	641	19230.
		24	29.0	1160	669	19401.
		25	29.0	1170	675	19575.
		26	28.0	1150	664	18592.
		27	29+0	1150	664	19256.
		28	27.0	1120	647	17469.
_		29	26.0	1080	625	16250.
·	SEP	30	29•0	1050	608	17632.

841.

TOTAL MONTHLY WEIGHTED T.D.S.

SUMMARY OF WATER QUALITY FOR THE

RIVERSIDE WATER QUALITY CONTROL PLANT

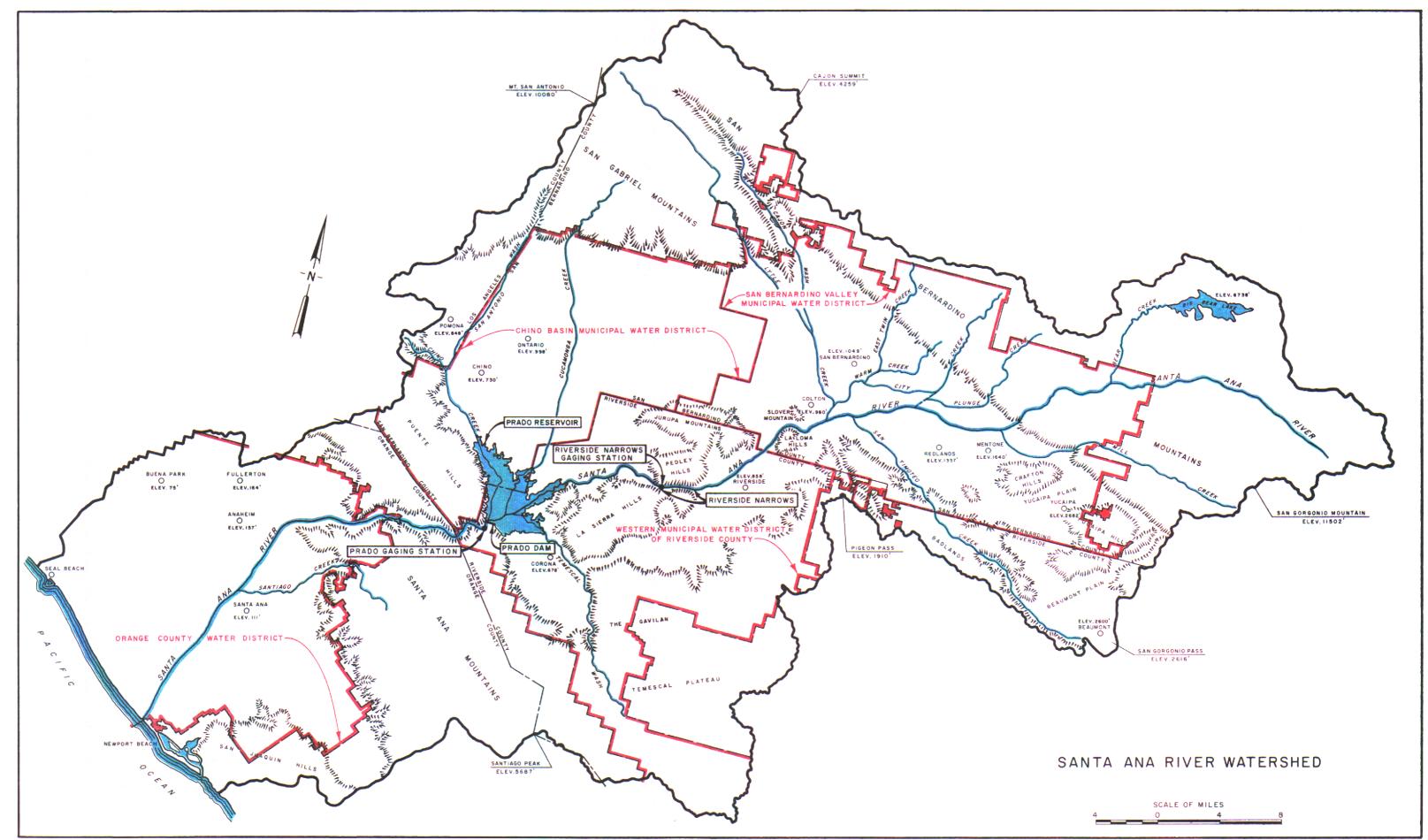
AT

RIVERSIDE NARROWS WATER YEAR 1973-74

Month	Monthly Flow Sec. Ft. Days	Mean Daily Flow Times Adjusted TDS	Average Monthly TDS	
	·			
October	836	510,844	611	
November	797	471,038	591	
December	777	417,746	538	
January	815	477,591	586	
Februar y	719	495,452	689	
March	822	520,919	634	
April	803	561,114	699	
May	875	539,784	617	
June	864	567,146	656	
July	844	569,074	674	,
August	869	576,532	663	
September	841	546,966	650	
				•
Totals	9,862	6,254,206	<u> </u>	
Total A.F.	19,561			·

Note: Monthly totals from Table No. 4.

Weighted Average Annual TDS at the
Riverside Quality Control Plant = 6,254,206 = 634 ppm



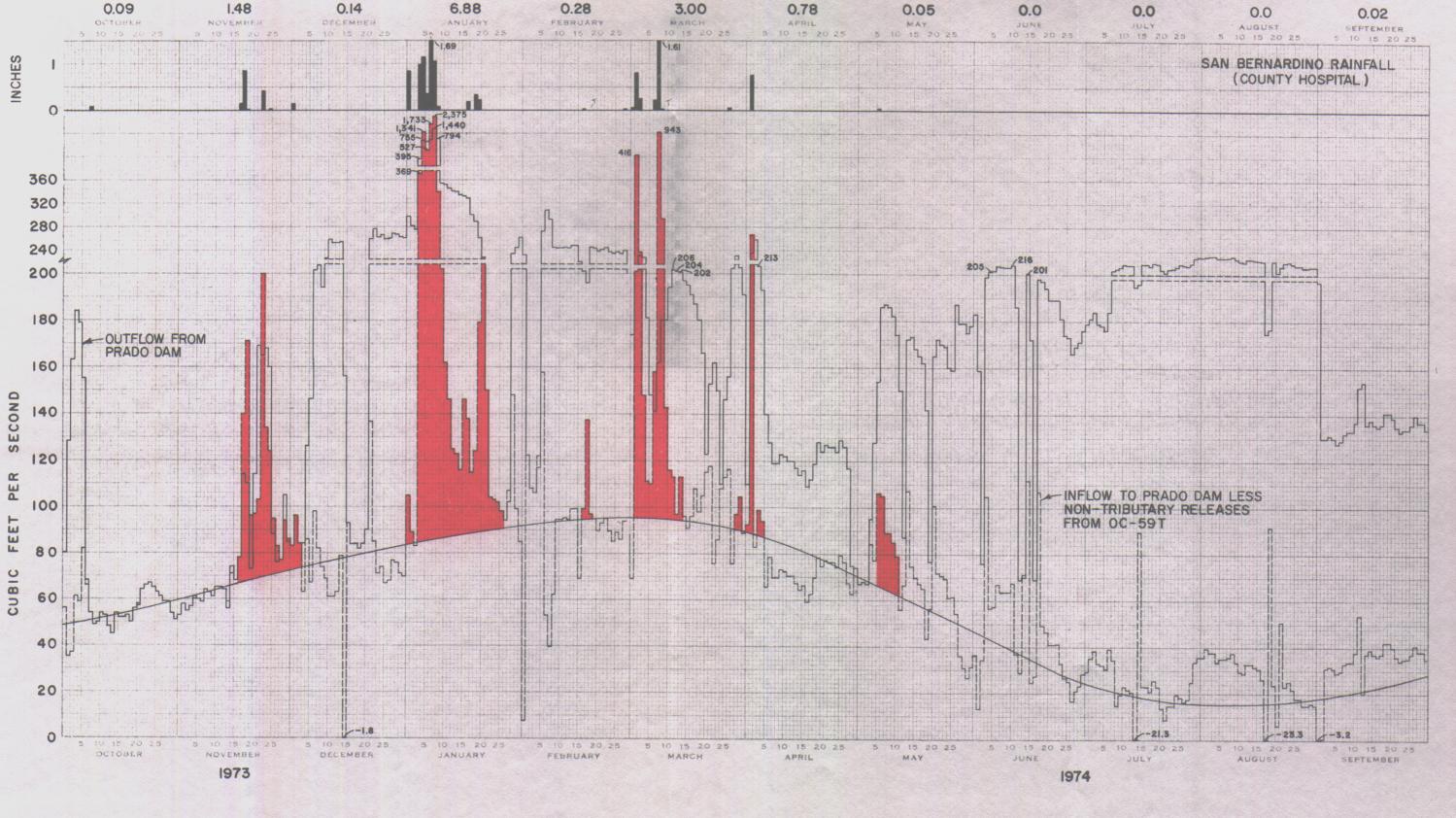
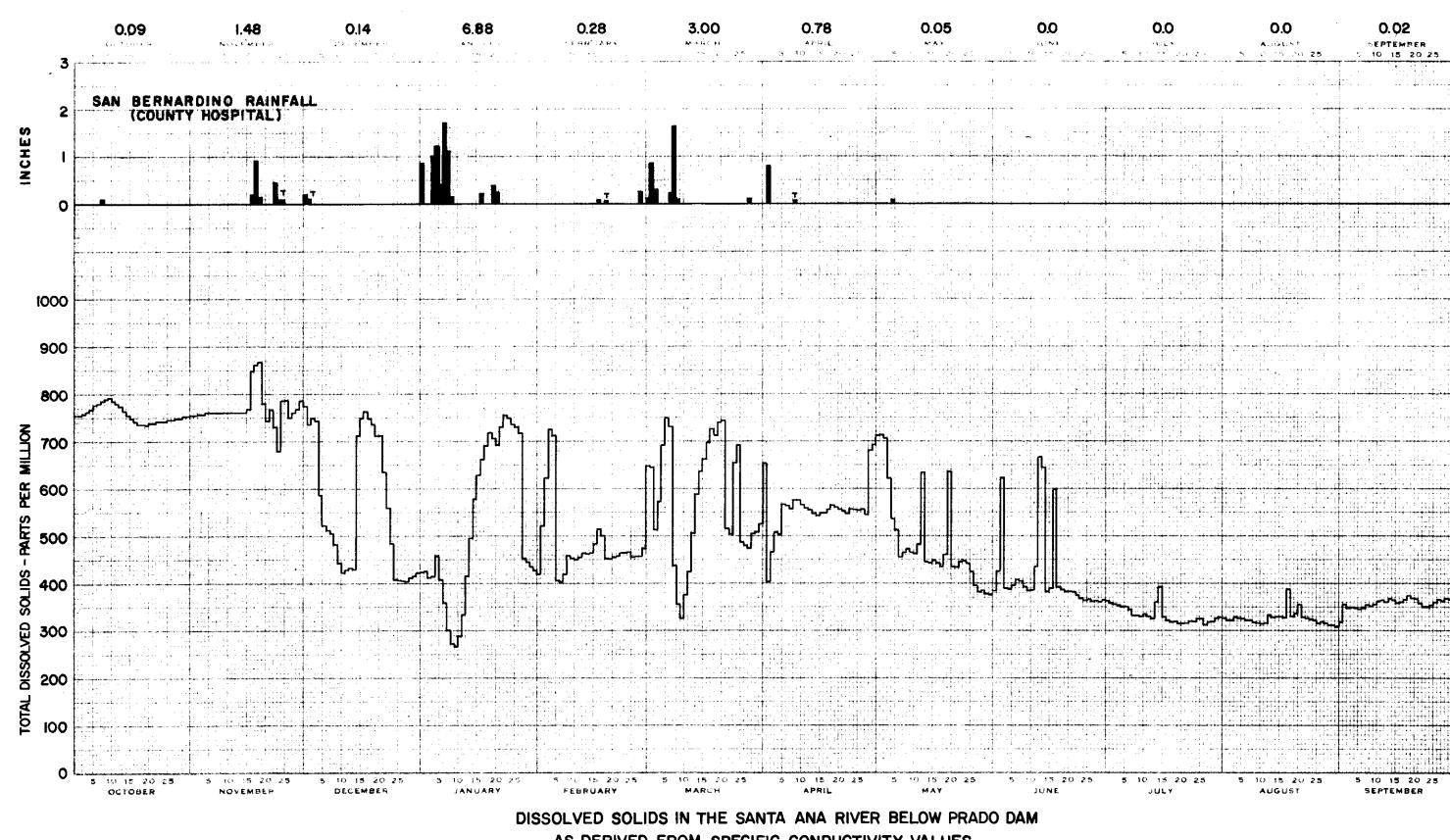
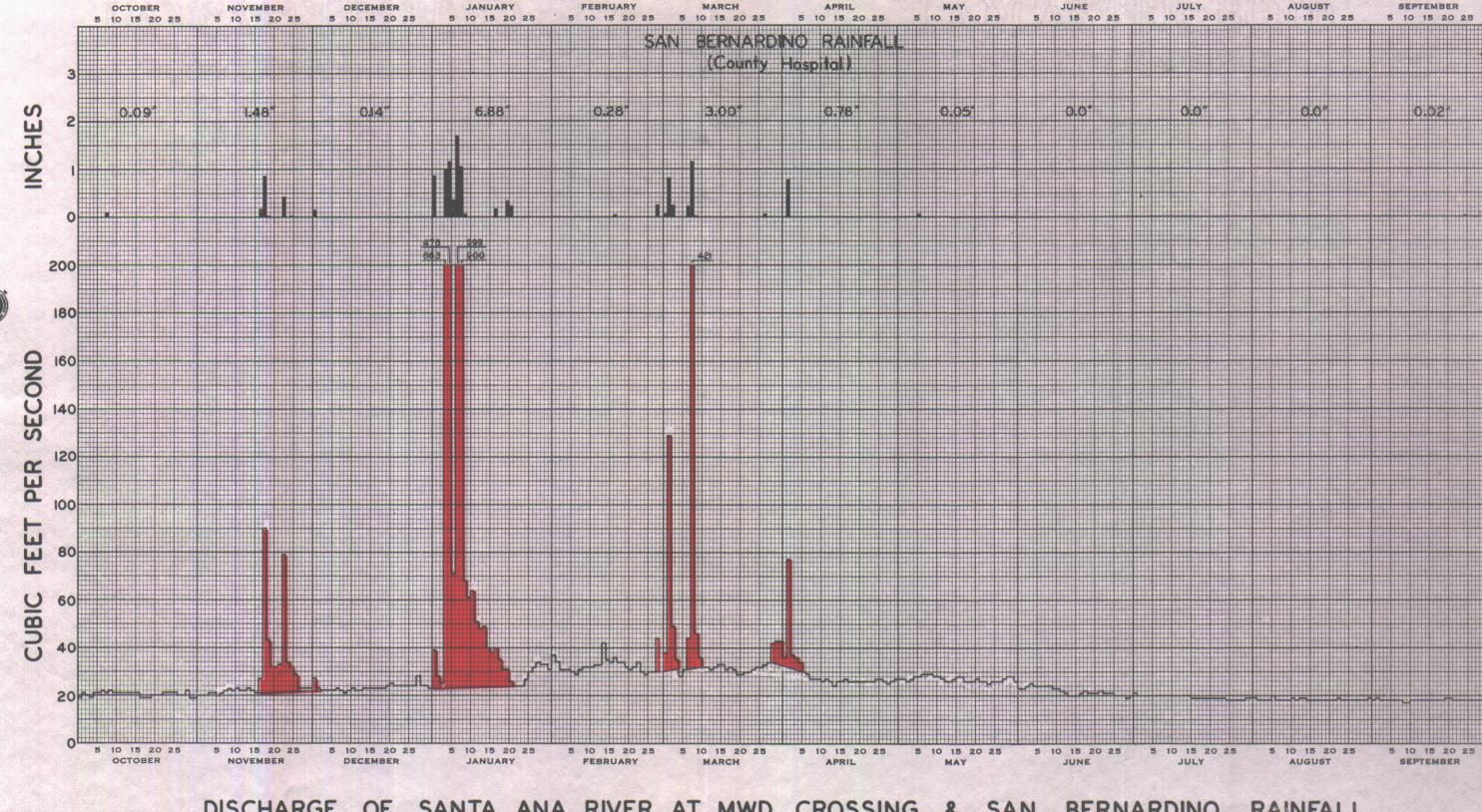


PLATE 2 (WATER YEAR 1973-74)



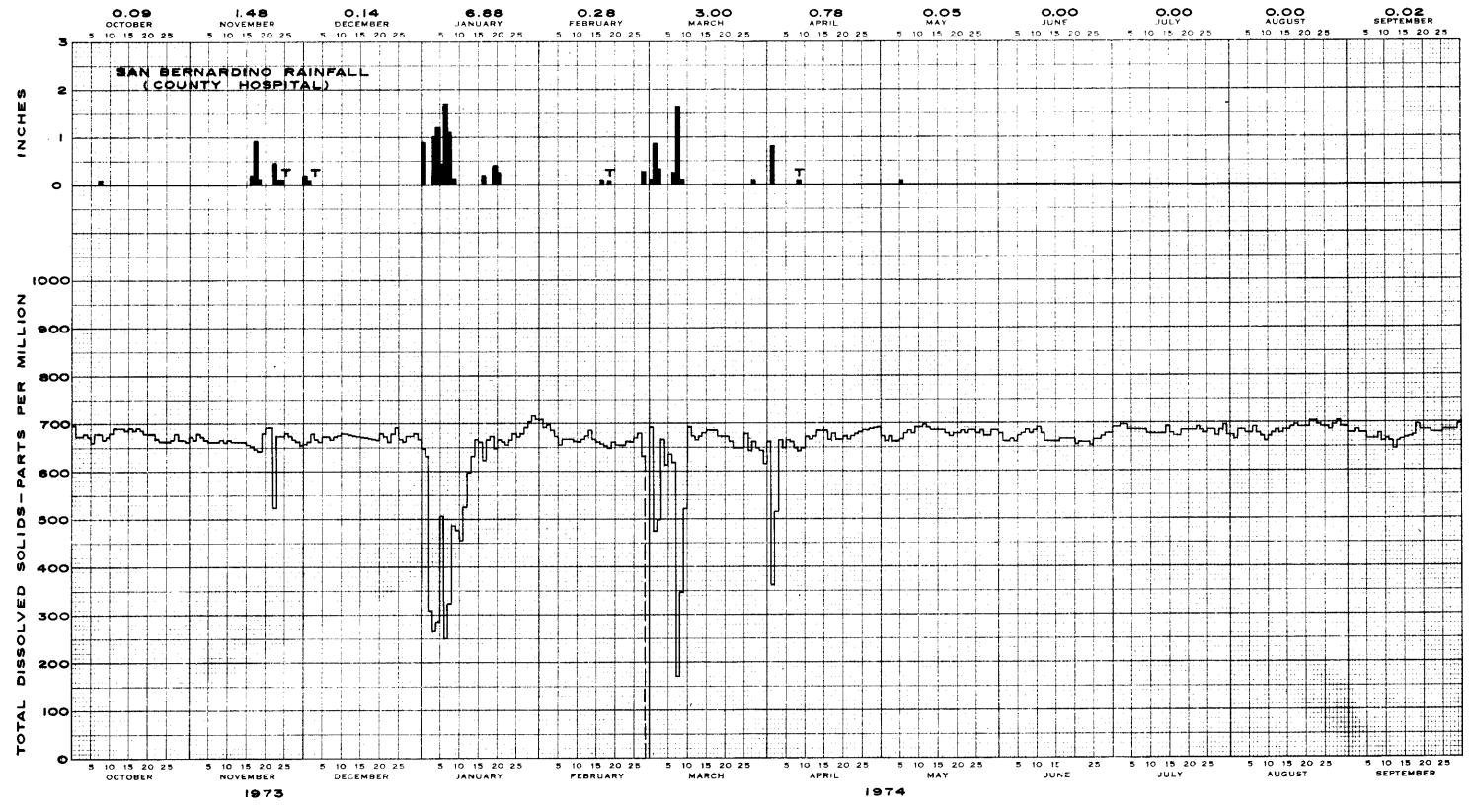
ISSOLVED SOLIDS IN THE SANTA ANA RIVER BELOW PRADO DAM
AS DERIVED FROM SPECIFIC CONDUCTIVITY VALUES
MEASURED BY THE USGS MONITORING STATION

PLATE 3 (WATER YEAR 73/74)



DISCHARGE OF SANTA ANA RIVER AT MWD CROSSING & SAN BERNARDINO RAINFALL

(WATER YEAR 1973 - 1974)



TOTAL DISSOLVED SOLID IN THE SANTA ANA RIVER AT RIVERSIDE NARROWS

UPPER FEEDER CROSSING OF M.W.D. AS DERIVED FROM

SPECIFIC CONDUCTIVITY VALUES MEASURED BY THE U.S.G.S. MONITORING STATION

PLATE 5 (WATER YEAR 1973-74)